

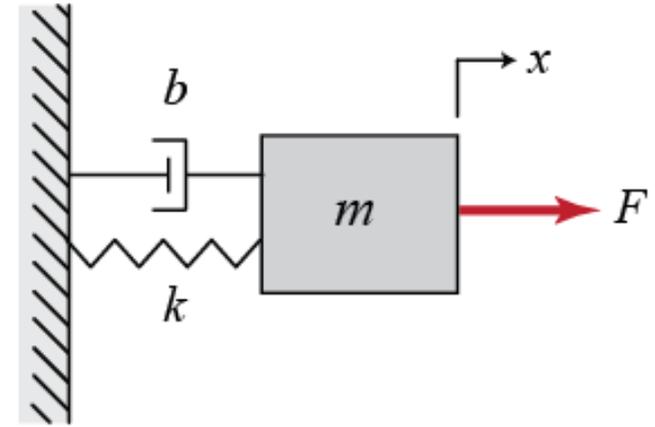
## Exercise 1

Suppose we have a simple mass, spring, and damper problem. Find

1. The modeling equation of this system ( $F$  input,  $x$  output).
2. The transfer function.

Let  $M = 1$  kg  $b = 10$  N s/m  $k = 20$  N/m  $F = 1$  N

3. Find Open-Loop Step Response.
4. Design a proportional controller to improve the output ( $\omega_n=17.89$ ).
5. Design a proportional derivative controller to improve the output ( $\zeta=0.56$  and  $\omega_n=17.89$ ).



## Solution 1

1. The modeling equation of this system

$$\sum f = M \frac{d^2 x}{dt^2}$$

$$M\ddot{x} = -b\dot{x} - kx + F \Rightarrow M\ddot{x} + b\dot{x} + kx = F$$

2. The transfer function.

Taking the Laplace transform of the modeling equation, we get

$$Ms^2X(s) + bsX(s) + kX(s) = F(s) \Rightarrow G(s) = \frac{X(s)}{F(s)} = \frac{1}{Ms^2 + bs + k}$$

Let  $M = 1$  kg  $b = 10$  N s/m  $k = 20$  N/m  $F = 1$  N

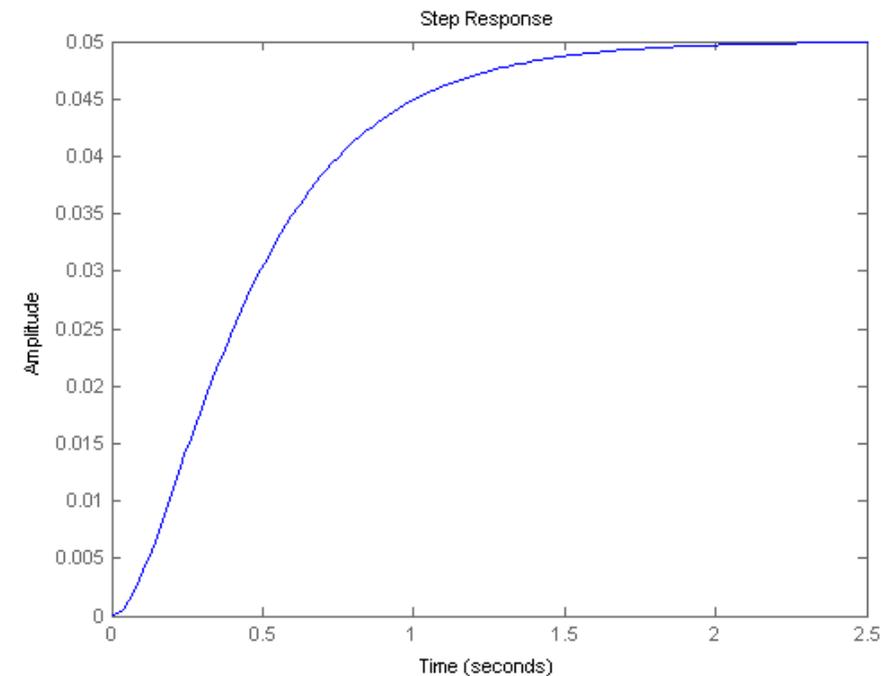
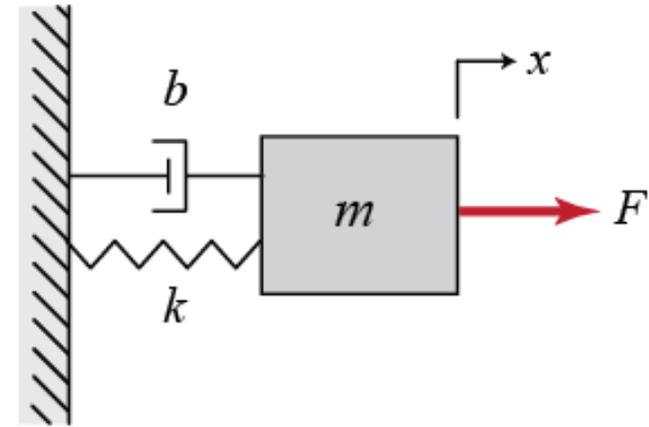
Plug these values into the above transfer function  $G(s) = \frac{X(s)}{F(s)} = \frac{1}{s^2 + 10s + 20}$

3. Find Open-Loop Step Response.

Create a new m-file (Matlab) and run the following code:

```
s = tf('s');  
P = 1/(s^2 + 10*s + 20);  
step(P)
```

- the DC gain of the plant transfer function is  $1/20$ , so 0.05 is the final value of the output to an unit step input.
- this corresponds to the steady-state error of 0.95, quite large indeed.
- the rise time is about one second,
- the settling time is about 1.5 seconds

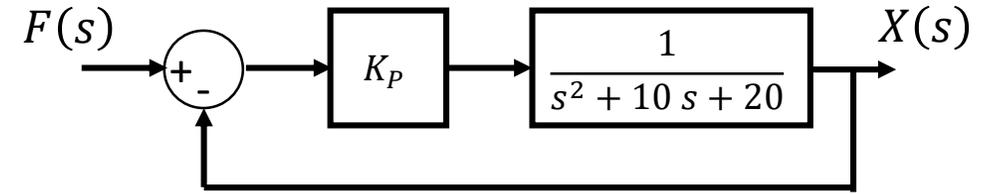


## 4. Proportional Control

The proportional controller ( $K_p$ ) reduces the rise time, increases the overshoot, and reduces the steady-state error.

$$G(s) = \frac{X(s)}{F(s)} = \frac{K_p}{s^2 + 10s + (20 + K_p)}$$

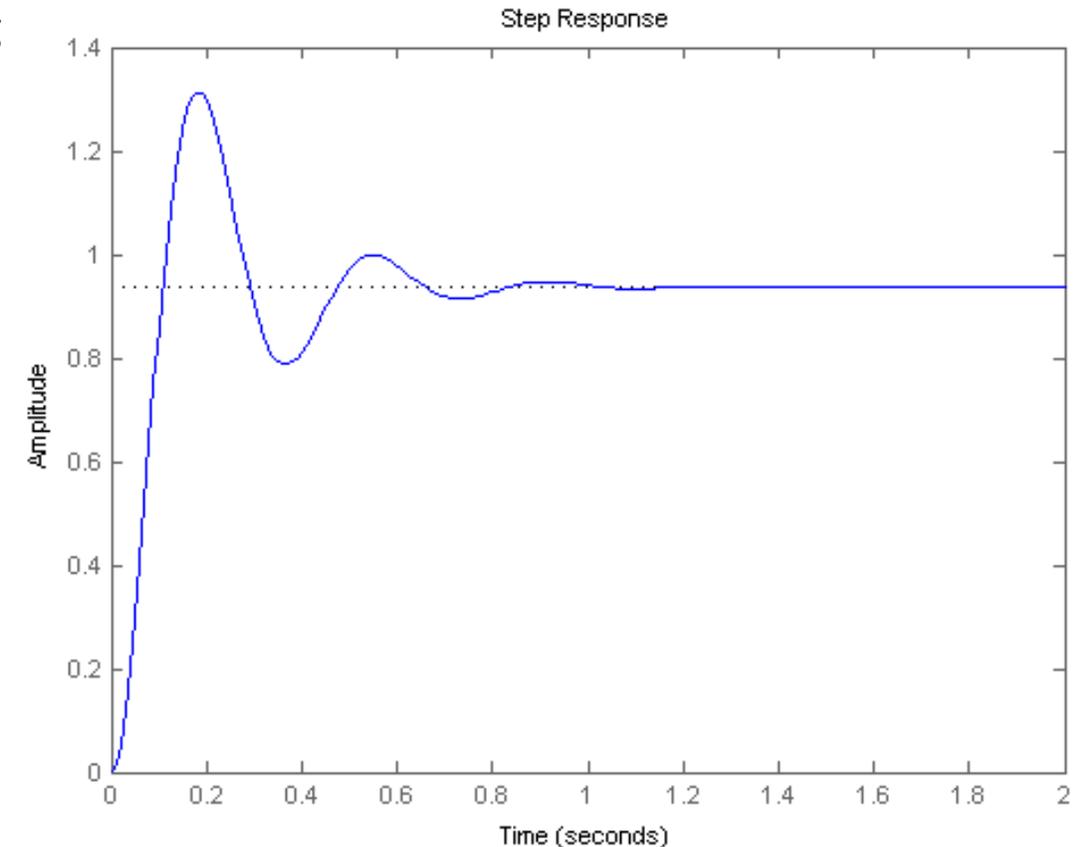
$$\omega_n^2 = 20 + K_p \Rightarrow K_p = \omega_n^2 - 20 = 300$$



Let the proportional gain equal 300 and change the m-file to the following

```
Kp = 300;  
C = pid(Kp)  
T = feedback(C*P,1)  
  
t = 0:0.01:2;  
step(T,t)
```

The above plot shows that the proportional controller reduced both the rise time and the steady-state error, increased the overshoot, and decreased the settling time by small amount.



## Proportional-Derivative Control

Now, let's take a look at a PD control. From the table shown above, we see that the derivative controller ( $K_d$ ) reduces both the overshoot and the settling time. The closed-loop transfer function of the given system with a PD controller is:

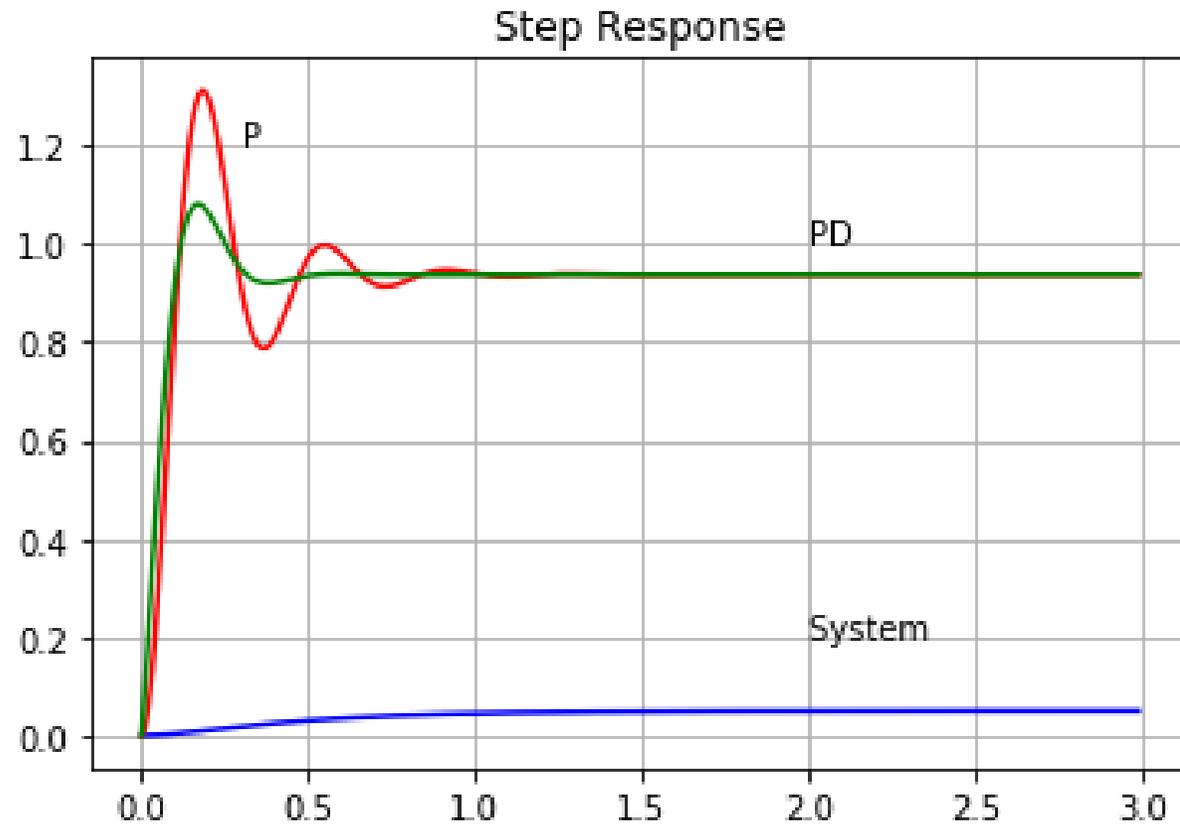
$$20 + K_P = \omega_n^2 \Rightarrow K_P = \omega_n^2 - 20 = 300$$

$$10 + K_D = 2\zeta\omega_n \Rightarrow K_D = 2\zeta\omega_n - 20 = 2(0.56)(17.89) - 20 \Rightarrow K_D = 10$$

```
Kp = 300;  
Kd = 10;  
C = pid(Kp,0,Kd)  
T = feedback(C*P,1)  
  
t = 0:0.01:2;  
step(T,t)
```

This plot shows that the derivative controller reduced both the overshoot and the settling time, and had a small effect on the rise time and the steady-state error.

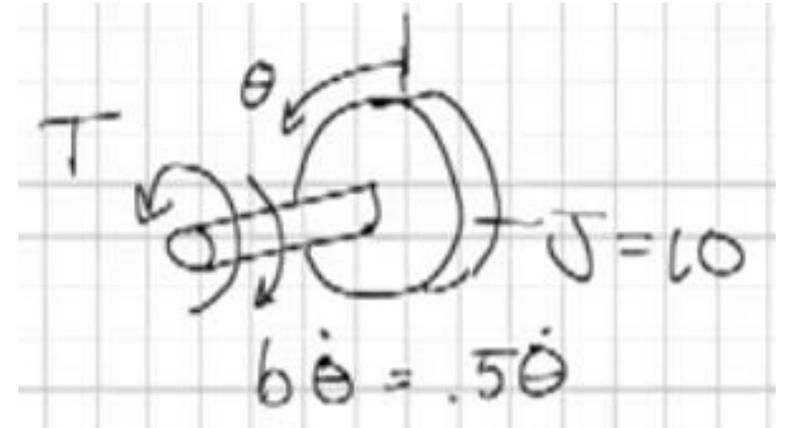
$$\frac{X(s)}{F(s)} = \frac{K_d s + K_p}{s^2 + (10 + K_d)s + (20 + K_p)}$$



## Exercise 2

The plant consists of rotating mass with inertia  $J$  and a viscous friction  $b$ , a torque  $T$  is applied to control the position of the mass.

1. Find the system model.
2. Find the transfer function.
3. Control the position  $\theta$  using  $T$  to have  $\zeta = 0.7$  (Proportional controller)

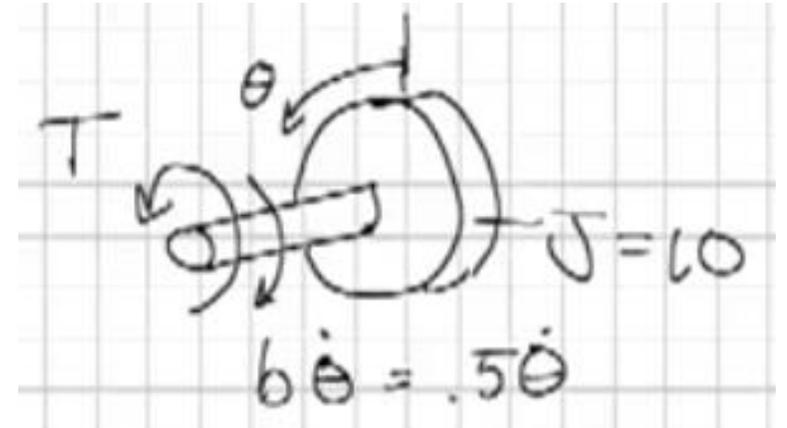


## Solution 2

1. The modeling equation of this system

$$\sum \text{Torques} = J \frac{d^2 \theta}{dt^2}$$

$$J\ddot{\theta} = T - b\dot{\theta} \Rightarrow J\ddot{\theta} + b\dot{\theta} = T \Rightarrow \ddot{\theta} + 0.05\dot{\theta} = 0.1T$$



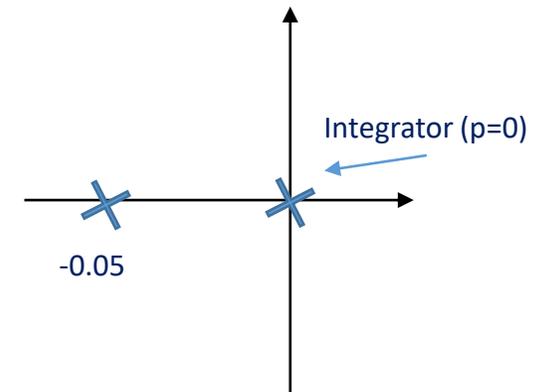
2. The transfer function

$$s^2 \theta(s) + 0.05 s \theta(s) = 0.1 T(s) \Rightarrow \frac{\theta(s)}{T(s)} = \frac{0.1}{s^2 + 0.05 s}$$

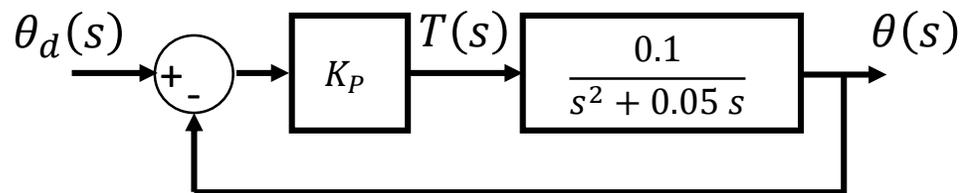
3. System control

The open Loop Analysis

$$t_s = \frac{4}{\sigma} = \frac{4}{0.05} = 80 \text{ sec (very slow moving system)}$$



The close-Loop with Proportional controller Analysis



$$\frac{\frac{0.1K_P}{s^2 + 0.05 s}}{1 + \frac{0.1K_P}{s^2 + 0.05 s}} = \frac{0.1K_P}{s^2 + 0.05 s + 0.1K_P}$$

Given the characteristic equation we calculate the value of  $K_P$  to have the desired transient response

$$CLCE : s^2 + 0.05 s + 0.1K_P$$

$$CLCE \text{ Desired} : s^2 + 2\zeta\omega_n s + \omega_n^2$$

Matching

$$2\zeta\omega_n = 0.05$$

$$0.1K_P = \omega_n^2$$

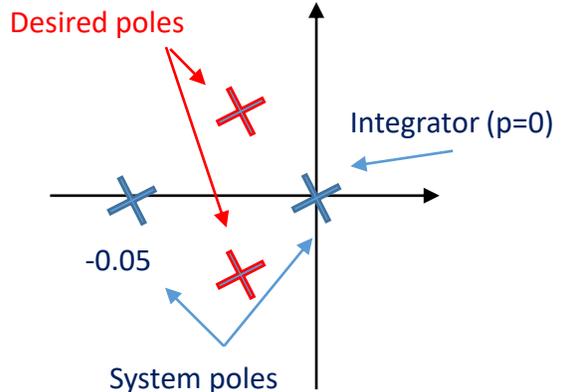


$$\omega_n = \frac{0.05}{2(0.7)} = 0.0357 \text{ rad/sec}$$

$$K_P = 10(0.0357)^2 = 0.0127$$

The desired specifications:  $\zeta = 0.7$

$$\text{The desired poles: } P_{1,2} = -\zeta\omega_n \pm j\omega_n\sqrt{1-\zeta^2} = -0.025 \pm j0.025$$



## Exercise 2

The plant  $G(s)$  is given  $G(s) = \frac{10}{s^2 - 3s + 2}$ , design a PD controller (using pole placement) to have the desired system response:  $\xi = 0.5$ , and  $T_s = 1s$

1. Find the desired poles and give the PD controller transfer function  $G_c(s)$  (general form).
2. Find the closed loop transfer function CLTF (with PD controller).
3. Find the closed loop characteristic equation CLCE.
4. Find the gains  $K_D$  and  $K_P$  of the PD controller.

## Solution

1. desired poles at :  $T_s = \frac{4}{\xi\omega_n} \rightarrow \omega_n = \frac{4}{\xi T_s} = 8 \text{ rad/sec}$

$$s_{1,2} = -\xi\omega_n \pm \omega_n\sqrt{1-\xi^2} = -4 \pm j 6.93$$

PD controller transfer function:  $G_c(s) = K_P + K_D s$

2. CLTF :  $T(s) = \frac{G_c(s)G(s)}{1+G_c(s)G(s)} = \frac{10(K_P+K_D s)}{s^2+(10K_D-3)s+10K_P+2}$

3. CLCE:  $s^2+(10K_D-3)s+10K_P+2=0$

4. Desired CLCE:  $s^2+2\xi\omega_n s+\omega_n^2=0$

PD controller Gains:  $K_P = \frac{\omega_n^2-2}{10}$  and  $K_D = \frac{2\xi\omega_n+3}{10}$

$$K_P = 6.2 \text{ and } K_D = 1.1$$

### Exercise 3

Use a PI controller to control the system  $G(s) = \frac{2}{s+4}$  to meet the specifications  $\zeta = 0.7$  and  $t_s < 0.5 \text{ sec}$ .

## Solution

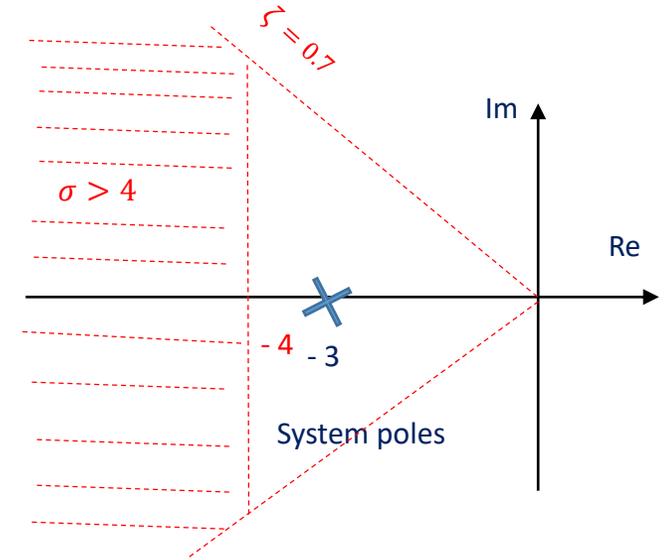
The system is type zero, it has no integrator. In order to have no steady-state error we need to add an integrator to make the system type one.

The open Loop Analysis: the system pole at  $p = -3$ .

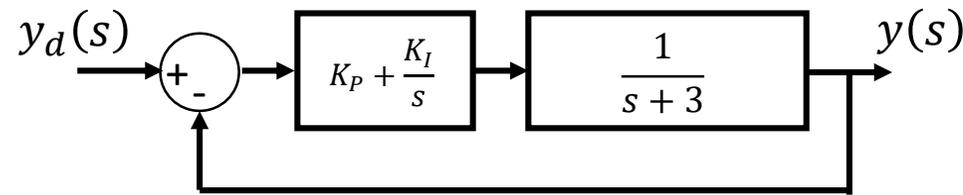
$$\zeta = 0.7.$$

$$t_s = \frac{4}{\sigma} < 1 \quad \Rightarrow \quad \sigma = \zeta \omega_n > 4 \quad \Rightarrow \quad \omega_n > \frac{4}{\zeta} = \frac{4}{0.7} \quad \Rightarrow \quad \omega_n > 5.71 \quad \Rightarrow \quad \omega_n = 6$$

satisfy the settling time



The controller design: PI controller



The PI controller can be written as:

$$K_P + \frac{K_I}{s} = K_P \frac{\left(s + \frac{K_I}{K_P}\right)}{s}$$

Zero =  $K_{IP}$ 
Gain
Integrator

$$CLCE : s(s + 3) + K_P \left(s + \frac{K_I}{K_P}\right) = 0 \quad \Rightarrow \quad s^2 + (2 + K_P)s + K_I = 0$$

$$Desired CLCE : s^2 + 2\zeta\omega_n s + \omega_n^2 = s^2 + 2(0.7)(6)s + (6)^2 = s^2 + 8.4s + 36 = 0$$

$$\Rightarrow \left. \begin{array}{l} 2 + K_P = 8.4 \\ K_I = 36 \end{array} \right\} \Rightarrow \left\{ \begin{array}{l} K_P = 7.4 \\ K_I = 36 \end{array} \right.$$