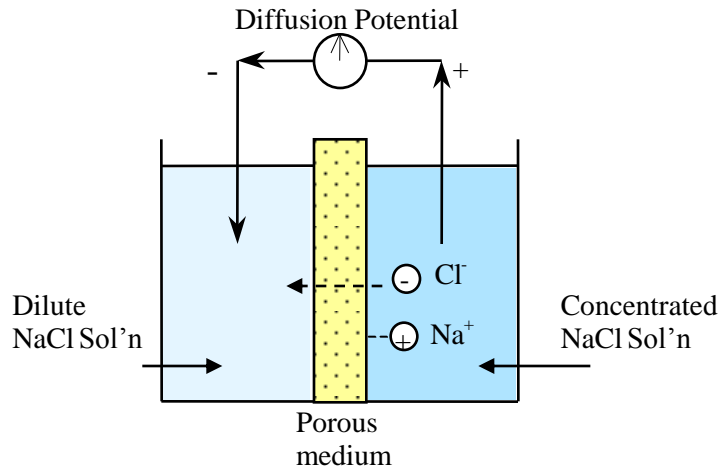
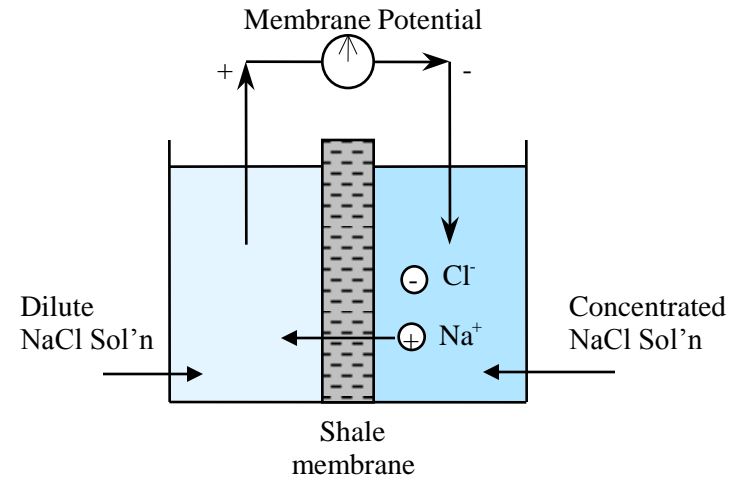


Definition of Potential Cells



Schematic of diffusion-potential generating cell

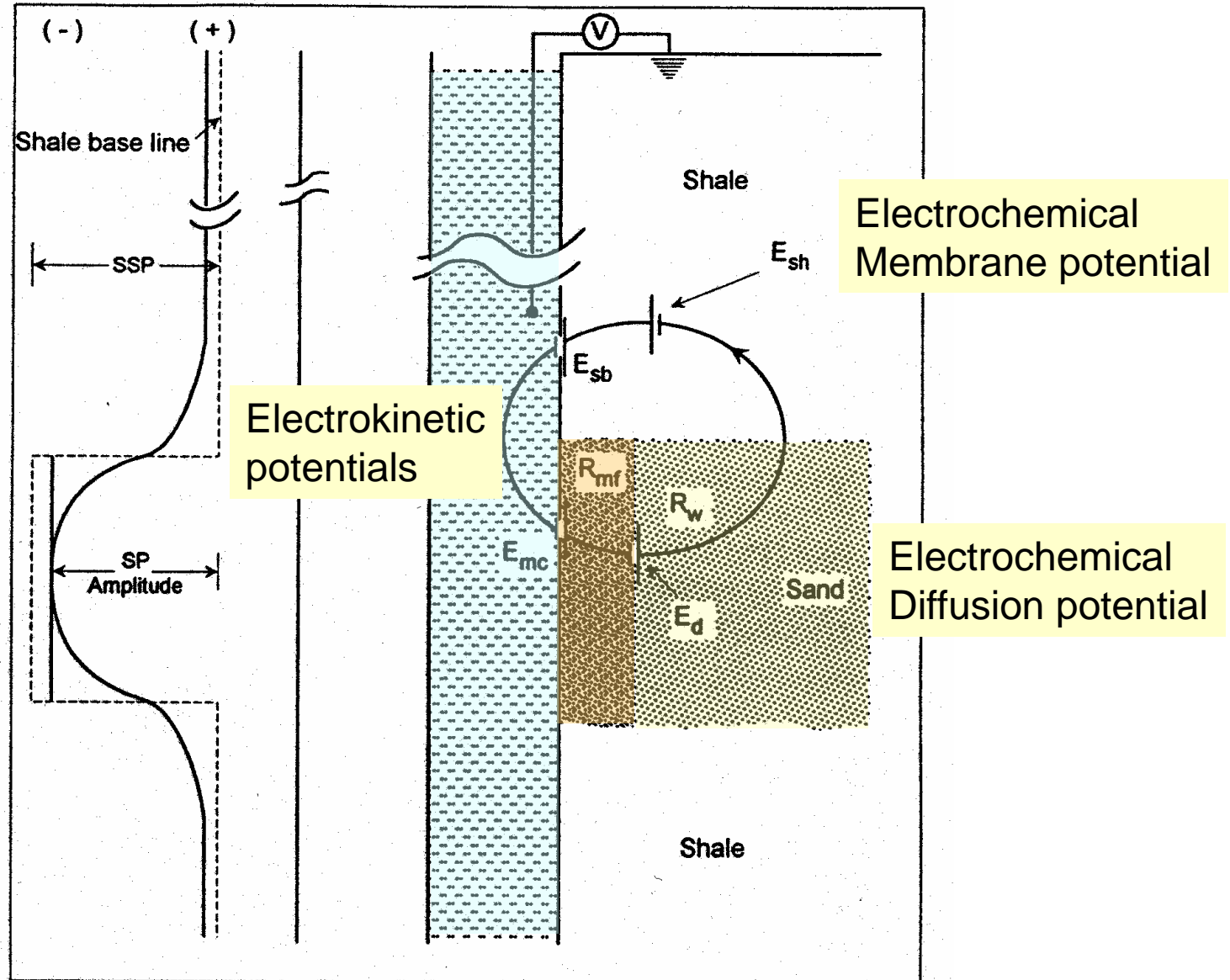


Schematic of a membrane-potential generating cell

SP Log

Background

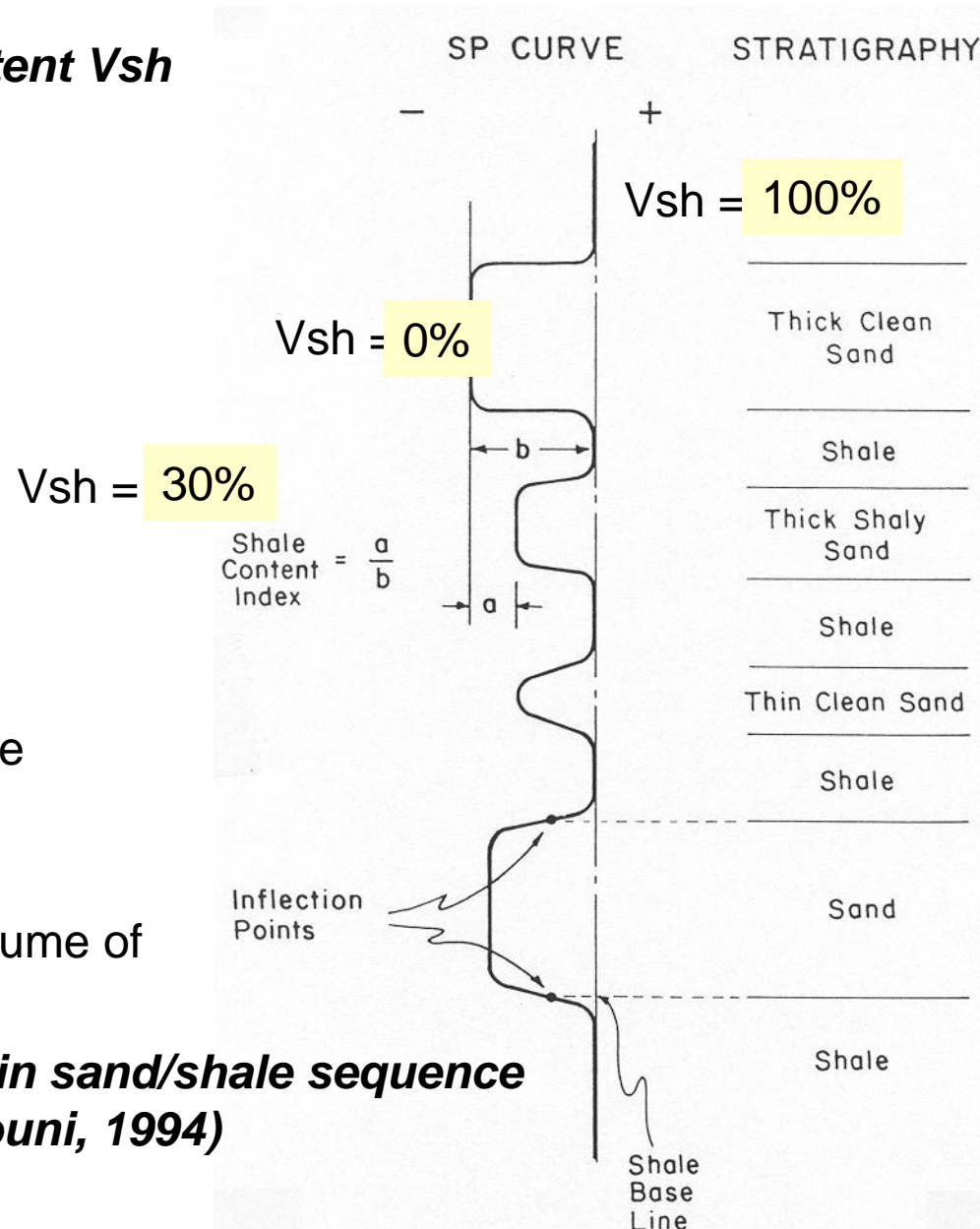
Origin of SP Curve



The SP log is used for:

- A. Identifying permeable bed boundaries
- B. Stratigraphic correlations
- C. Determination of formation resistivity factor, F
- D. Estimation of shale content (V_{sh}) for shaly sand formations.
- E. Determination of formation water resistivity, R_w
- F. All of the above

Estimation of shale content V_{sh}



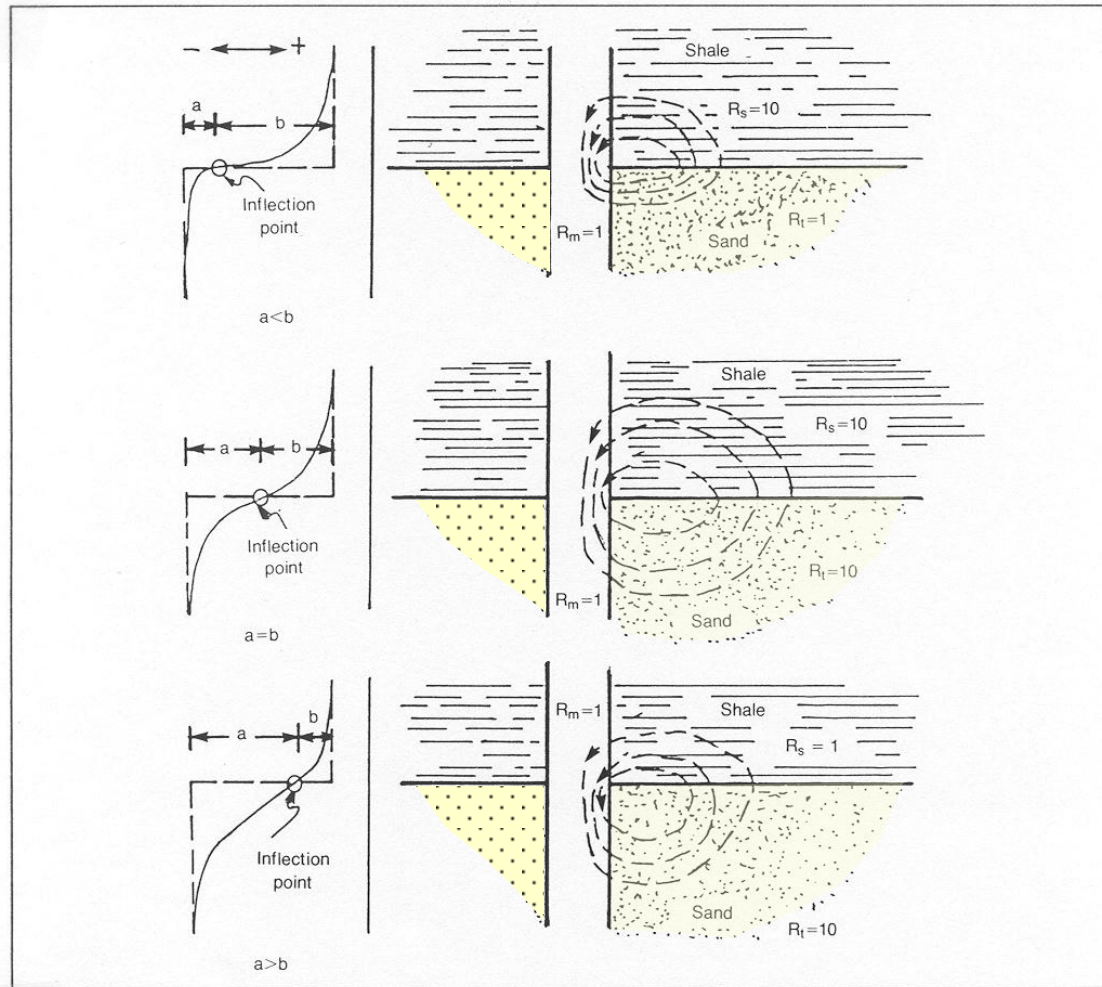
Assumptions

zones of same salinity, shale type....

Typically, overestimates volume of shale

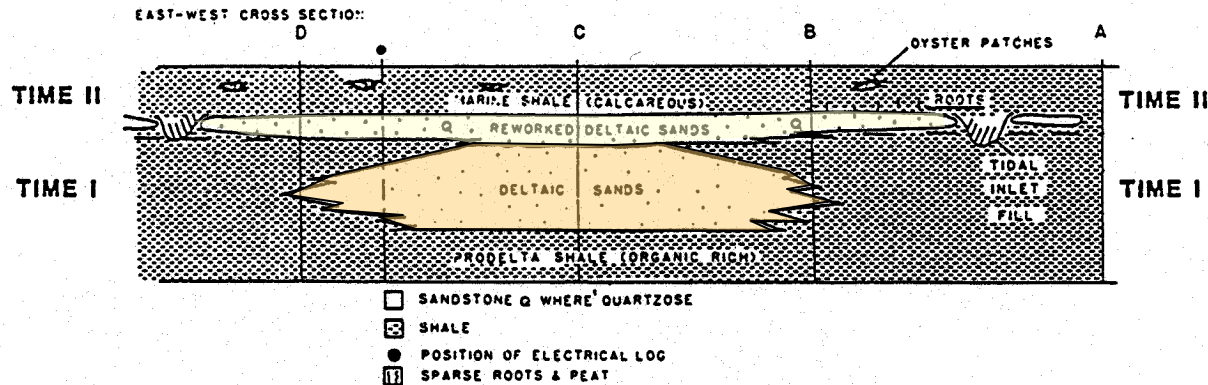
Schematic SP curve in sand/shale sequence
(Bassiouni, 1994)

Identification of boundaries (Helander, 1983)

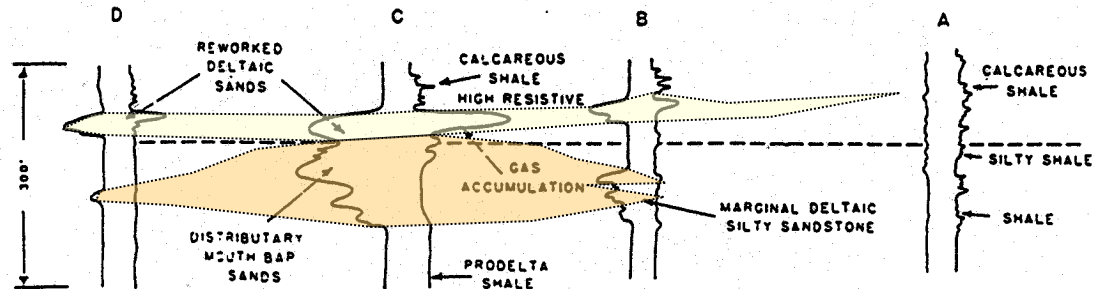


SP shape as a function of current distribution

Stratigraphic Correlation



Depositional model for reworked deltaic sands. (A) Plan view setting, (B) Cross section geometry. Note the thickness variations and the differences of areal extent between the lower deltaic sands and the upper reworked sands.

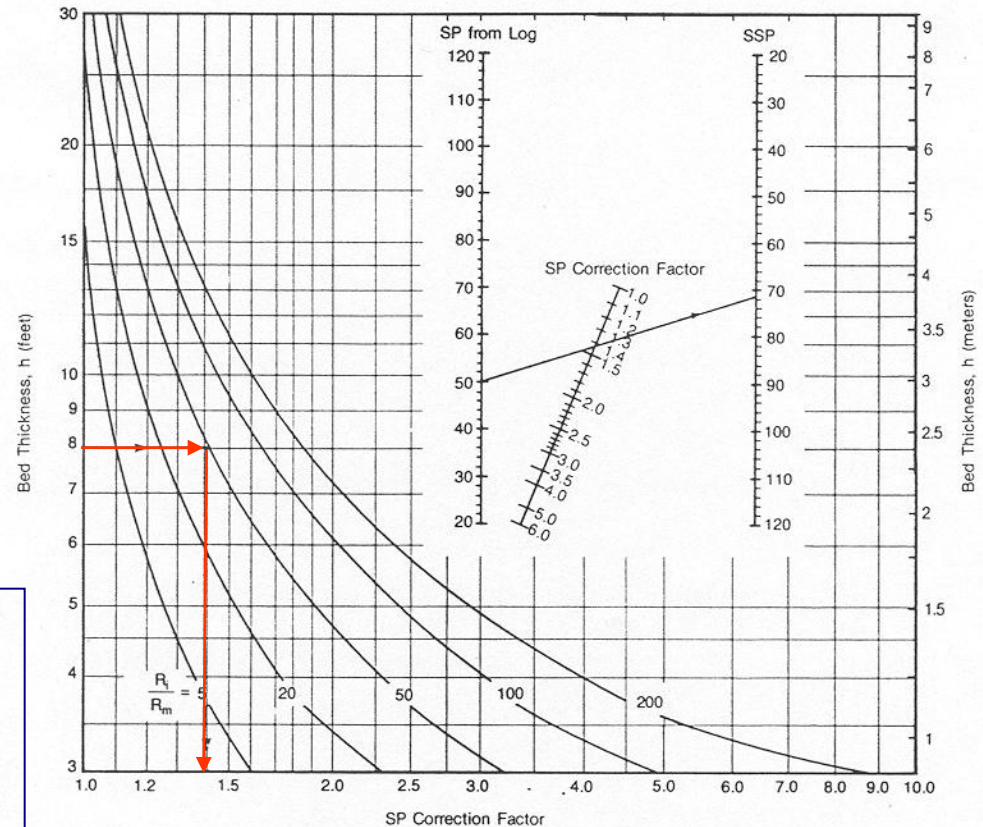


An electric log cross section showing the lateral variation of sandstones in the reworked deltaic setting. This cross section is keyed to the lithologies in above. (After Saxena, 1979)

Procedure to Obtain Rw

- Identify the shale baseline and clean sand lines on the SP log. The difference is SP.
- Calculate the formation temperature
- Convert $(R_{mf})_{T_m} \Rightarrow (R_{mf})_{T_f}$
- If necessary, correct SP for bed thickness and invasion effects. Read bed thickness, h and invaded resistivity, R_i . Obtain SSP.
- If necessary, Convert $R_{mf} @ T_f$ to $R_{mfe} @ T_f$.
- Calculate R_{we} by:
$$R_{we} = R_{mfe} * 10^{\left(\frac{SSP}{61 + 0.133T_f} \right)}$$
- Convert R_{we} to R_w .

Bed thickness/invasion correction (Western Atlas, 1992)



$$SP \text{ correction factor} = \frac{\left\{ 4 \left(\frac{R_i}{R_m} + 2 \right) \right\}^{\frac{1}{3.65} - 1.5}}{h - \left\{ \left(\frac{R_i}{R_m} + 11 \right) / 0.65 \right\}^{\frac{1}{6.05} - 0.1}} + 0.95$$

for $\frac{R_i}{R_m} > 5$ and $3 < h < 50$, for h in feet.

$$SSP = SP \times SP \text{ correction factor}$$

Example:

Given: $SP_{log} = -50$ mV; $h = 8$ ft; $R_i = 35 \Omega m$; $R_m = 0.7 \Omega m$

Solution: Bed thickness = 8 ft; $R_i/R_m = 50$; SP correction factor = 1.42

Nomograph Solution: $SP_{log} = -50$ mV; SP correction factor = 1.42; $SSP = -71$ mV

Gamma Ray and Spontaneous Potential

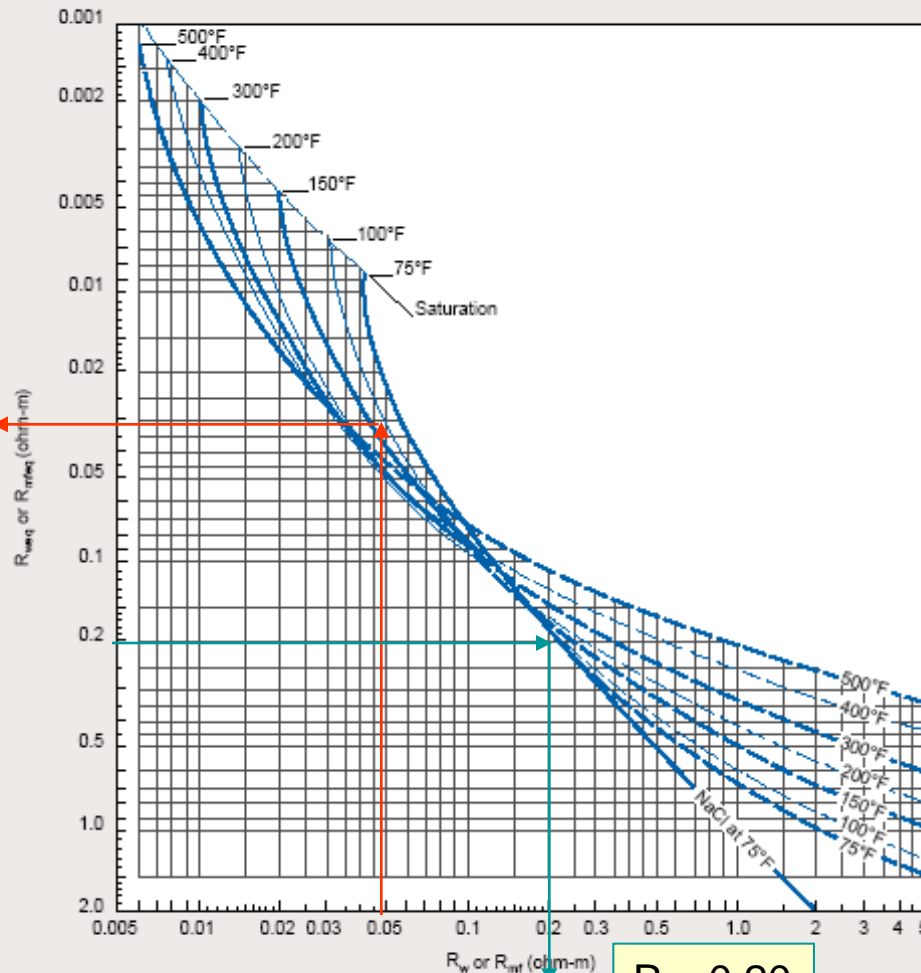
Schlumberger

R_w versus R_{weq} and Formation Temperature

SP-2
(English)

SP

$R_{mfe}=0.03$



$R_w=0.20$

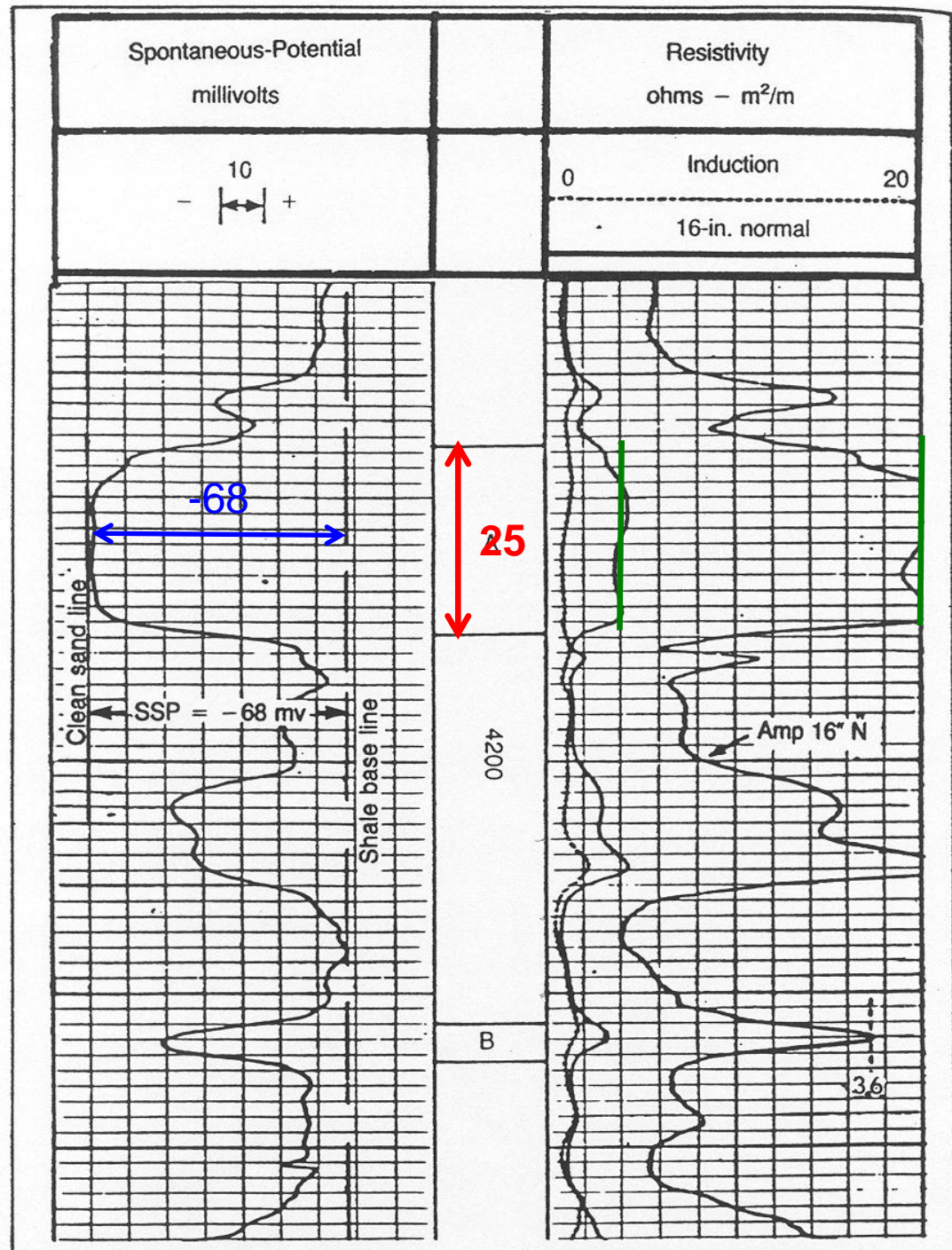
SP Log

Example

SP = -68 mV

Ri = 4 ohmm

H = 25 ft



Example

The example is a SP - resistivity log over a series of sands and shales. Referring to the figure, compute R_w for zone A. The following information is given:

TTD= 196 deg F @ TD = 9,400 ft.

Gulf Coast well

$R_{mf} = 0.71$ @ $T_m = 68$ deg. F

$R_m = 1.00$ @ $T_m = 68$ deg. F

Step 1: Determine the SP value as the difference between the shale baseline and the thick, clean sand line. The shale line is taken as the maximum SP excursion to the right. The sand line is taken as the maximum deflection to the left in the zone of interest.

Step 1: *The shale baseline and clean sand line are drawn on the figure.*

$SP = -68$ mV is the potential difference.

Step 2: The formation temperature is obtained by linear interpolation between the mean surface temperature and the recorded bottomhole temperature from the log.

Example

Step 2: *The formation temperature can be computed by:*

$$T_f = (196 - 75) \frac{4170}{9400} + 75 = 129^\circ F$$

Step 3: The R_{mf} and R_m at a measured temperature from the log heading, must be converted to formation temperature.

Step 3: *The R_{mf} at formation temperature is:*

$$(R_{mf})_f = 0.71 \left(\frac{68 + 6.77}{129 + 6.77} \right) = 0.39 \Omega - m$$

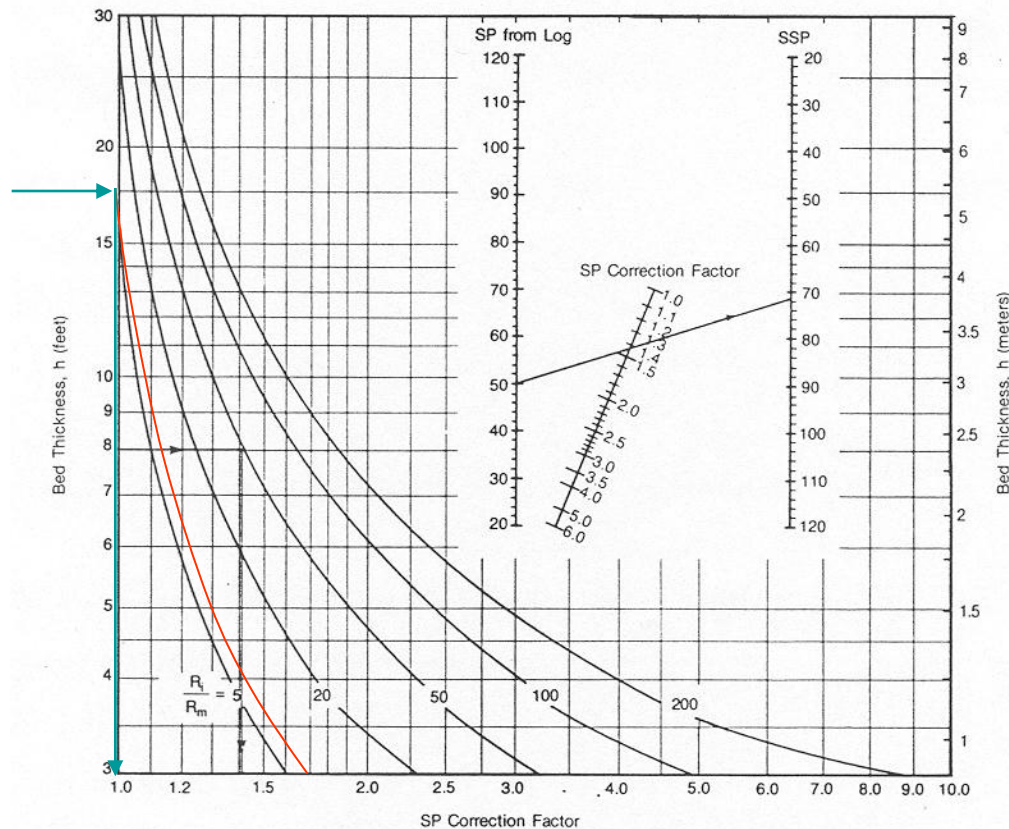
Similarly, $R_m = 0.55 \text{ ohm-m @ } T_f$

Step 4: The SP reading must be corrected for bed thickness and resistivity effects. Thin beds and deep invasion reduce the amplitude of the SP to less than the desired SSP. Enter the figure with the bed thickness and invaded-zone resistivity from a short normal, SFL or LL8 and estimate the correction factor.

Example

Step 4: Bed thickness = 25ft.; $R_i = 4$ ohm-m from the 16" short normal; thus $R_i/R_m = 7.2 \approx 7.5$.

From the figure the correction factor = 1.00.



Example

Step 5: The mud filtrate resistivity (R_{mf}) at formation temperature calculated from Step 3, must be corrected to R_{mfe} , for use in the SSP equation. The term equivalent is a result of two assumptions in formulating the SSP equation:

- (1) formation water and mud filtrate are NaCl solutions, and
- (2) activity ratios can be replaced by resistivity ratios.

Use the figure to convert from $R_{mf} \rightarrow R_{mfe}$ and from $R_{we} \rightarrow R_w$
(Do not use the dashed lines, they are for gyp-based muds).

SP Log

Application-Rw

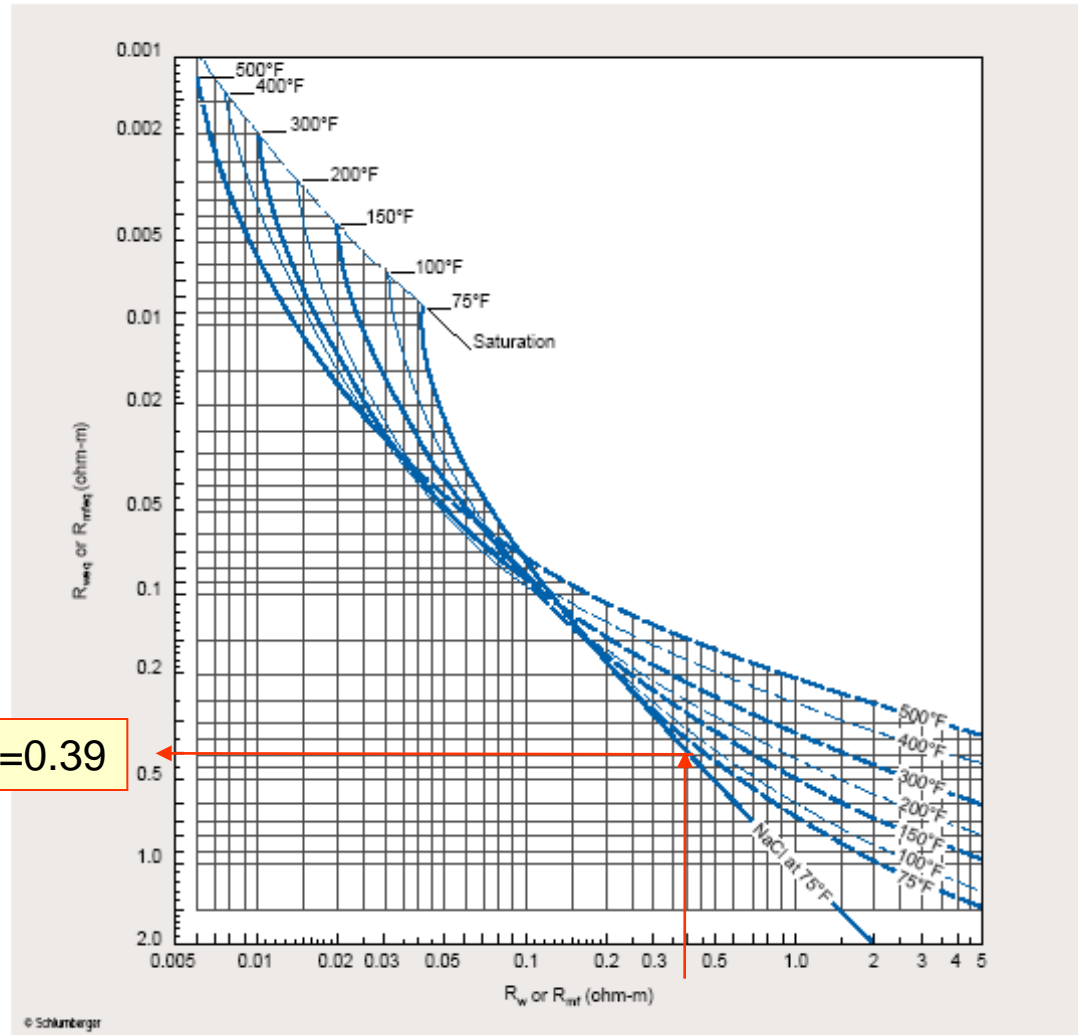
Step 5: Since $R_{mf} > 0.25$ then $R_{mfe} = R_{mf} = 0.39 \text{ ohm-m}$.

Schlumberger

SP-2
(English)

SP

$R_{mfe} = 0.39$



Example

Step 6: Calculate Rwe by using:

$$R_{we} = R_{mfe} * 10^{\left(\frac{SSP}{61+0.133T} \right)}$$

Step 6: Calculate the equivalent formation water resistivity.

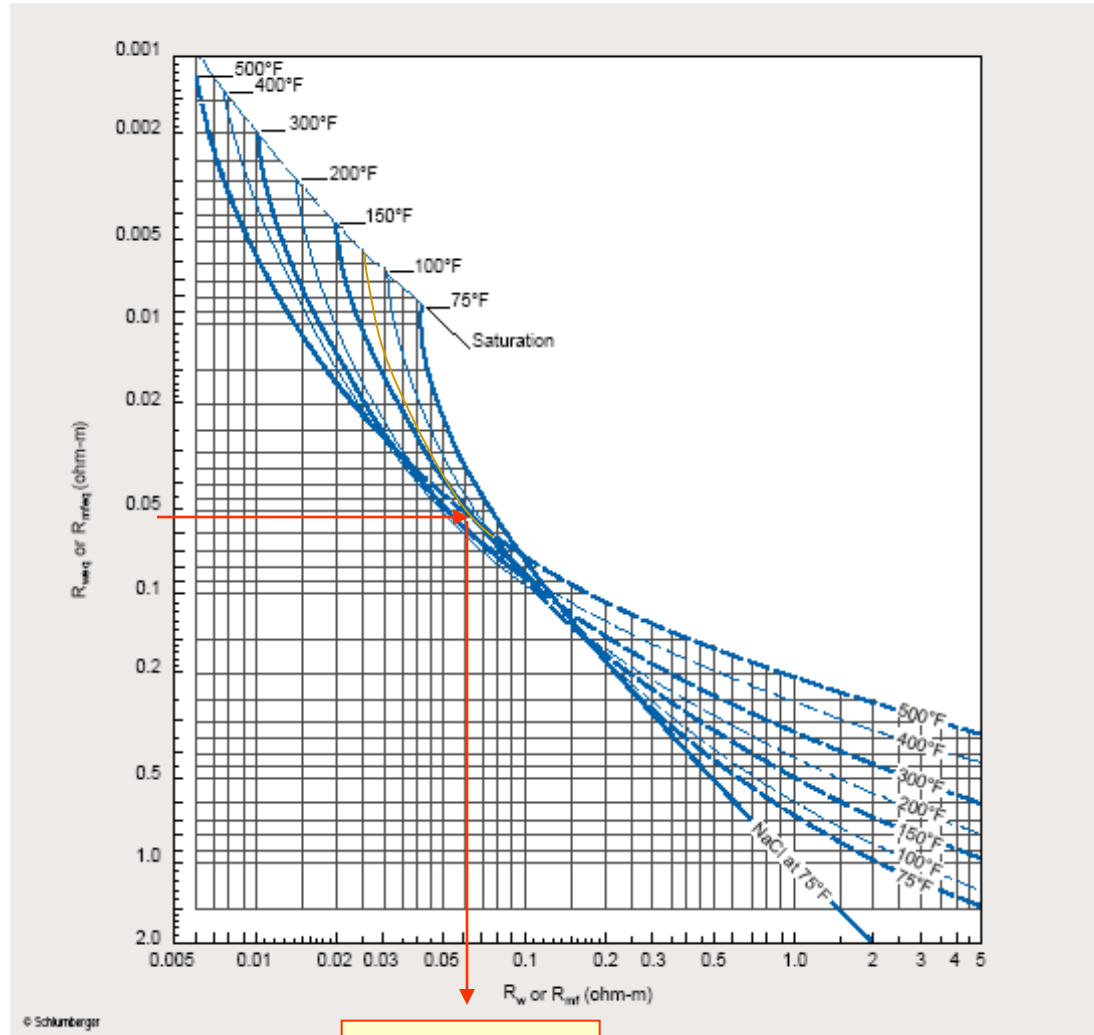
$$R_{we} = 0.39 * 10^{\left(\frac{-68}{61+0.133(129)} \right)} = 0.052 \Omega - m$$

Step 7: Use the equivalence conversion chart to convert Rwe to Rw.

Example

Step 7:

$R_w = 0.060 \text{ ohm-m}$

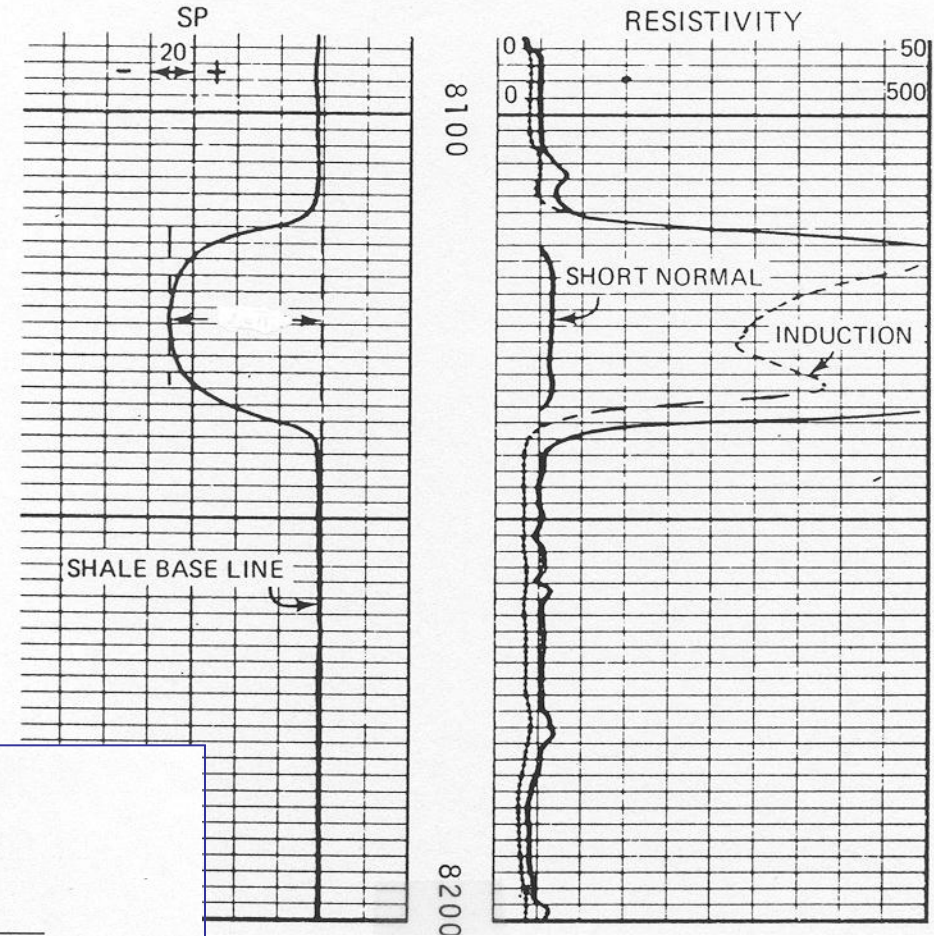


$R_w = 0.06$

SP Log

Exercise

Well Log Heading Data: Formation - Morrow sandstone
 $R_{mf} = 2.0 @ 70^{\circ}F$ surface temp. = 60°
 $R_m = 2.5 @ 70$ TD temp. 164 TD = 10500



SP ALGORITHM

1. T_{TD} _____ TD _____ T_o _____ T_f _____
2. $R_{mf} =$ _____ @ _____ F $R_m =$ _____ @ _____ F $R_{mf} @ T_f =$ _____
 $R_m @ T_f =$ _____
3. SP from log _____ mV.
4. Bed thickness _____ ft.
5. SP correction R_i _____ R_i/R_m _____ correction factor _____
 $SSP = \frac{\text{c.f.}}{\text{SP}} * \text{SP} =$ _____
6. $R_{mfe} =$ _____
7. $R_{we} =$ _____
8. $R_w =$ _____