

IE-352
Section 1, CRN: 48700/1/2
Section 2, CRN: 48706/7/8
Second Semester 1435-36 H (Spring-2015) – 4(4,1,2)
“MANUFACTURING PROCESSES – 2”

Thursday, April 23, 2015 (04/07/1436H)

MIDTERM 2 [10 POINTS]

Name:	Student Number:	Section:
	4	10 / 11

Place the correct letter in the box at the right of each question [$\frac{1}{2}$ Point Each]

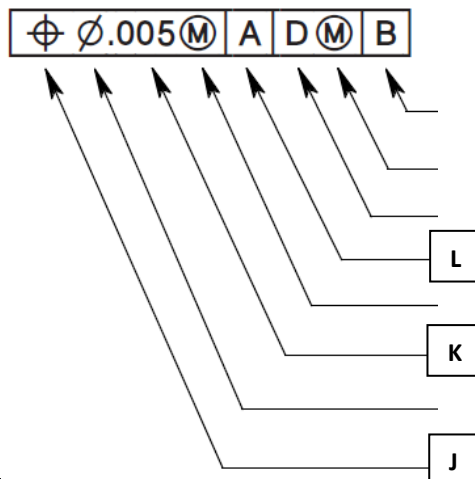
- Classify, respectively, the following geometric symbols: // , ≡ , — :

 - A. orientation, form, location
 - B. form, orientation, location
 - C. orientation, location, form
 - D. location, form, orientation
 - E. location, orientation, form

- Respectively, the following geometric symbols: // , ≡ , — stand for,

 - A. parallelism, symmetry, straightness
 - B. symmetry, parallelism, straightness
 - C. parallelism, symmetry, flatness
 - D. symmetry, parallelism, flatness
 - E. flatness, symmetry, straightness

Questions 3-4. Examine the feature control frame shown below and answer the questions to follow.



3. How do you read the feature control frame shown above?

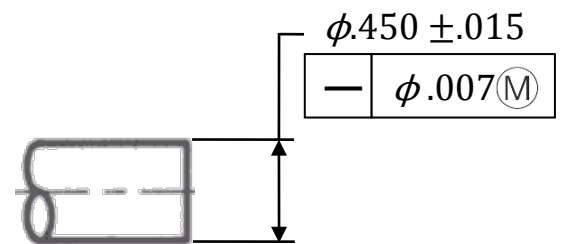
- A. position GT of feature (*RFS*) is 0.005-diam. cylind. zone relative to datums *A, D, B*
- B. circularity GT of feature (*RFS*) is 0.005-diam. cylind. zone relative to datums *A, D, B*
- C. position GT of feature at *LMC* is 0.005-diam. cylind. zone relative to datums *A, D, B*
- D. circularity GT of feature at *MMC* is 0.005-diam. cylind. zone relative to datums *A, D, B*
- E. position GT of feature at *MMC* is 0.005-diam. cylind. zone relative to datums *A, D, B*

4. Respectively, the symbols *J, K, and L* stand for,

- A. *J*: geometric characteristic symbol, *K*: geometric tolerance, *L*: tertiary datum
- B. *J*: geometric characteristic symbol, *K*: basic size, *L*: primary datum
- C. *J*: diameter symbol, *K*: geometric tolerance, *L*: primary datum
- D. *J*: geometric characteristic symbol, *K*: geometric tolerance, *L*: primary datum
- E. *J*: diameter symbol, *K*: basic size, *L*: tertiary datum

5. For the system shown below, $GT_{LMC} =$

- A. 0.037
- B. 0.007
- C. 0.015
- D. 0.014
- E. 0.030



6. Repeat P5 above given *no* material condition

modifier is defined in the *FCF*.

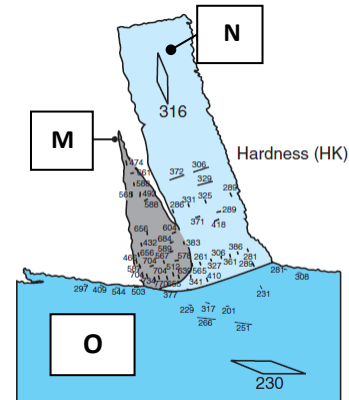
- A. 0.037
- B. 0.007
- C. 0.015
- D. 0.014
- E. 0.030

7. The following process involves a rotating workpiece and radially inward tool:

- A. cutting off
- B. slab milling
- C. drilling
- D. end milling
- E. turning

8. Label the hardness distribution diagram shown below.

- A. **M**: BUE; **N**: continuous chip; **O**: tool
- B. **M**: continuous chip; **N**: BUE; **O**: tool
- C. **M**: BUE; **N**: continuous chip; **O**: workpiece
- D. **M**: continuous chip; **N**: BUE; **O**: workpiece
- E. **M**: serrated chip; **N**: continuous chip; **O**: workpiece



9. Discontinuous chips form under ALL of the following conditions,

- A. high α , large t_0 , very high V , high machine tool stiffness
- B. low α , small t_0 , normal V , low machine tool stiffness
- C. high α , large t_0 , normal V , low machine tool stiffness
- D. low α , small t_0 , very high V , high machine tool stiffness
- E. low α , large t_0 , very high V , low machine tool stiffness

10. Respectively, the following can be used to measure cutting forces, temperature,

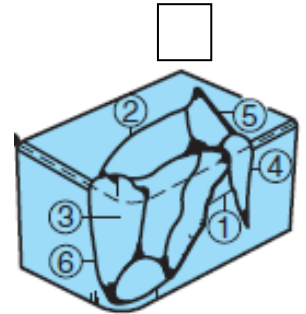
- A. acoustic emission transducer, dynamometer
- B. dynamometer, acoustic emission transducer
- C. radiation pyrometer, dynamometer
- D. dynamometer, radiation pyrometer
- E. radiation pyrometer, acoustic emission transducer

11. Arrange the following parameters in *increasing* order of effect on tool life,

- A. f, t_0, V
- B. t_0, f, V
- C. V, t_0, f
- D. t_0, V, f
- E. V, f, t_0

12. Label the high-speed steel cutting tool diagram shown below.

- A. ① : crater wear; ② : flank wear; ③ : DOC line; ④ : failure face
- B. ① : failure face; ② : DOC line; ③ : flank wear; ④ : crater wear
- C. ① : flank wear; ② : failure face; ③ : DOC line; ④ : crater wear
- D. ① : flank wear; ② : crater wear; ③ : failure face; ④ : DOC line
- E. ① : DOC line; ② : crater wear; ③ : failure face; ④ : flank wear



Questions 13-20. In an orthogonal cutting operation using a ceramic tool ($n = 0.7$), $t_o = 0.25 \text{ mm}$, $V = 400 \text{ m/min}$, $\alpha = 15^\circ$, and $w = 8 \text{ mm}$. It is observed that $t_c = 0.45 \text{ mm}$, $F_c = 600 \text{ N}$, and the mean coefficient of friction in the cutting zone is 0.83.

13. What is the value of the *chip-compression factor*?

- A. 0.56
- B. 0.25
- C. 0.45
- D. 0.11
- E. 1.8

14. What is the value of the *shear angle*?

- A. 32.1°
- B. 57.9°
- C. 72.8°
- D. 49.3°
- E. 17.2°

15. What is the value of the *shear strain*?

- A. 3.27
- B. 1.72
- C. 1.90
- D. 3.54
- E. 2.22

16. What is the value of the *shear velocity*?

- A. 222 *m/min*
- B. 404 *m/min*
- C. 108 *m/min*
- D. 1314 *m/min*
- E. 723 *m/min*

17. What is the magnitude of the *thrust force*?

- A. 1305 *N*
- B. 80.2 *N*
- C. 4488 *N*
- D. 276 *N*
- E. 545 *N*

18. Find the required *source power* given a mechanical efficiency of 65%.

- A. 369 *kW*
- B. 4.0 *kW*
- C. 240 *kW*
- D. 2.6 *kW*
- E. 6.15 *kW*

19. What is the effect on *increase in mean temperature* of doubling the cutting speed?

- A. increase in T by 74%
- B. decrease in T by 74%
- C. increase in T by 26%.
- D. decrease in T by 26%
- E. increase in T by 41%

20. What is the effect on *tool life* of doubling the cutting speed?

- A. reduction in tool life by 37.1%
- B. reduction in tool life by 62.9%
- C. reduction in tool life by 61.6%
- D. reduction in tool life by 38.4%
- E. reduction in tool life by 50.0%

Equations, Data, Diagrams You May Find Useful

$$\log x^p = p \log x, \quad \log xy = \log x + \log y, \quad \log \frac{x}{y} = \log x - \log y$$

$$\tan \phi = \frac{r \cos \alpha}{1 - r \sin \alpha} \Rightarrow r = \frac{t_0}{t_c} = \frac{\sin \phi}{\cos(\phi - \alpha)} \quad \alpha_e = \sin^{-1}(\sin^2 i + \cos^2 i \sin \alpha_n)$$

$$r = \frac{t_0}{t_c} = \frac{V_c}{V}$$

$$\gamma = \frac{AB}{OC} = \frac{AO}{OC} + \frac{OB}{OC} \Rightarrow \gamma = \cot \phi + \tan(\phi - \alpha)$$

Shear Stress =

$$\frac{F_s}{\text{Area of the shear plane}}$$

$$\frac{V}{\cos(\phi - \alpha)} = \frac{V_s}{\cos \alpha} = \frac{V_c}{\sin \phi}$$

$$\phi = 45^\circ + \frac{\alpha}{2} - \frac{\beta}{2} \quad (\text{when } \mu = 0.5 \sim 2)$$

$$\Rightarrow \phi = 45^\circ + \alpha - \beta$$

$$T = \frac{0.000665 Y_f}{\rho c} \sqrt[3]{\frac{V t_0}{K}}$$

$$\text{Power} = F_c V$$

$$\text{Power for friction} = F V_c$$

$$\text{Power for shearing} = F_s V_s$$

$$VT^n d^x f^y = C$$

$$T = C^{1/n} V^{-1/n} d^{-x/n} f^{-y/n}$$

$$T \approx C^7 V^{-7} d^{-1} f^{-4}$$

$$R_t = \frac{f^2}{8R}$$

$$T_{\text{mean}} \propto V^a f^b$$

- Carbide tools: $a = 0.2, b = 0.125$
- High-speed steel tools: $a = 0.5, b = 0.375$

$$u_t = u_s + u_f \quad u_s = \frac{F_s V_s}{w t_0 V}$$

$$u_f = \frac{F V_c}{w t_0 V} = \frac{F r}{w t_0}$$

$$\eta_{\text{mech}} = \frac{\text{Power}_c}{\text{Power}_{\text{source}}}$$

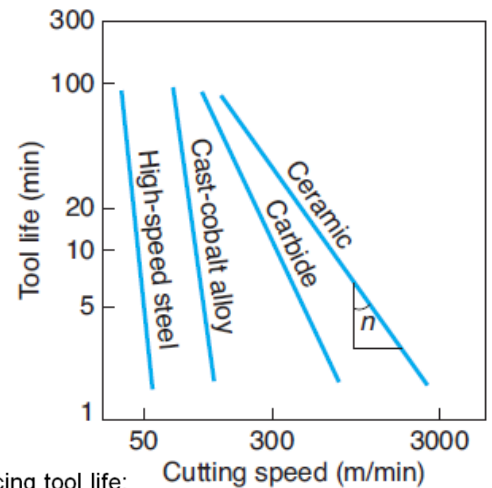
$$\mu = \tan \beta = \frac{F}{N} = \frac{F_t + F_c \tan \alpha}{F_c - F_t \tan \alpha}$$

$$F_s = F_c \cos \phi - F_t \sin \phi$$

$$F_n = F_c \sin \phi + F_t \cos \phi$$

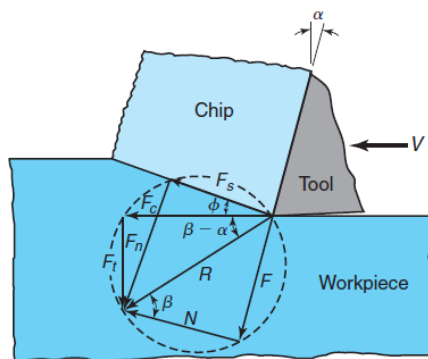
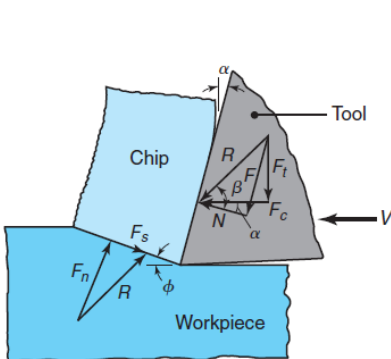
Ranges of n Values for the Taylor Equation (21.20a) for Various Tool Materials

High-speed steels	0.08–0.2
Cast alloys	0.1–0.15
Carbides	0.2–0.5
Coated carbides	0.4–0.6
Ceramics	0.5–0.7



- Recommended cutting speed is one producing tool life:
 - 60-120 min: high-speed steel tools
 - 30-60 min: carbide tools

$$F_t = R \sin(\beta - \alpha) \quad \text{or} \quad F_t = F_c \tan(\beta - \alpha)$$



Approximate Range of Energy Requirements in Cutting Operations at the Drive Motor of the Machine Tool (for Dull Tools, Multiply by 1.25)

Material	Specific energy $W \cdot s/mm^3$
Aluminum alloys	0.4–1
Cast irons	1.1–5.4
Copper alloys	1.4–3.2
High-temperature alloys	3.2–8
Magnesium alloys	0.3–0.6
Nickel alloys	4.8–6.7
Refractory alloys	3–9
Stainless steels	2–5
Steels	2–9
Titanium alloys	2–5