

IE-352

Section 1, CRN: 48700/1/2

Section 2, CRN: 48703/4/5

Section 3, CRN: 48706/7/8

Second Semester 1434-35 H (Spring-2014) – 4(4,1,2)




“MANUFACTURING PROCESSES – 2”

Sunday, April 27, 2014 (27/06/1435H)

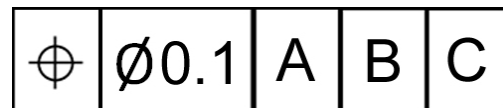
## HW 3 (MIDTERM 2)

Name:	Student Number: 4	Section: S/M8/M10
-------	----------------------	----------------------

Place the correct letter in the box at the right of each question [ $\frac{1}{2}$  Point Each]

1. **Classify, respectively, the following geometric symbols:** , , :
- A. location, form, location  
B. form, form, form  
C. location, location, location  
D. form, form, location  
E. location, form, form

**Questions 2-3.** Examine the feature control frame shown below and answer the questions to follow.



2. **How do you read the feature control frame shown above?**
- A. position GT of feature is a 0.1-diam. cylind. zone relative to datums A, B, C at  M
- B. position GT of feature is a 0.1-diam. cylind. zone relative to datums A, B, C at  L
- C. position GT of feature is a 0.1-diam. cylind. zone relative to datums A, B, C at  S
- D. cylindricity GT of feature is a 0.1-diam. cylind. zone relative to datum A, B, C at  M
- E. cylindricity GT of feature is a 0.1-diam. cylind. zone relative to datums A, B, C at  S

3. The feature control frame above can be used for a hole in which type of fit?

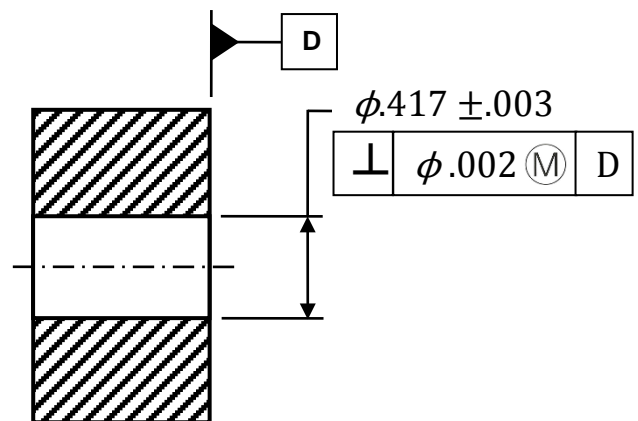
- A. interference fits
- B. clearance fits
- C. transition fits
- D. clearance or interference fits
- E. any type of fit

4. The major difference between flatness and parallelism tolerance for a plane is ...

- A. parallelism tolerance must have a material condition modifier
- B. parallelism tolerance must be defined relative to a datum
- C. parallelism tolerance must have a material modifier & be defined relative to a datum
- D flatness tolerance must be defined relative to a datum
- E. flatness tolerance must have a material condition modifier

5. For the system shown below,  $GT_{LMC} =$

- A. 0.002
- B. 0.003
- C. 0.005
- D. 0.006
- E. 0.008



6. Repeat P5 above given *no* material condition modifier is defined in the FCF.

- A. 0.002
- B. 0.003
- C. 0.005
- D. 0.006
- E. 0.008

7. Which of the following machining parameters is *always* smaller than unity ( $< 1$ )?

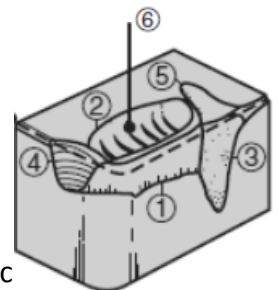
- A.  $r$  and  $\gamma$
- B.  $\mu$  and  $\gamma$
- C.  $r$  and  $\eta_{mech}$
- D.  $u_t$  and  $\eta_{mech}$
- E.  $\mu$  and  $u_t$

8. Which of the following machining parameters is not “unitless” (i.e. has units)?

- A.  $r$
- B.  $u_t$
- C.  $\gamma$
- D.  $\mu$
- E.  $\eta_{mech}$

9. Label the cutting tool diagram shown below

- A. ①: flank wear; ②: crater wear; ③: depth-of-cut line; ⑥: thermal cracks
- B. ①: crater wear; ②: flank wear; ③: depth-of-cut line; ⑥: thermal cracks
- C. ①: flank wear; ②: crater wear; ③: thermal cracks; ⑥: depth-of-cut line
- D. ①: flank wear; ②: thermal cracks; ③: depth-of-cut line; ⑥: crater wear
- E. ①: flank wear; ②: crater wear; ③: outer metal chip notch; ⑥: thermal crack



10. The *Taylor Tool Life* equation measures time to develop which type of wear?

- A.  $KT$
- B.  $R$
- C.  $VN$
- D.  $VB$
- E.  $VB_{max}$

11. Allowable notch wear is given by the symbol: ...

- A.  $KT$
- B.  $R$
- C.  $VN$
- D.  $VB$
- E.  $VB_{max}$

12. Maximum crater wear is given by the following symbol: ...

- A.  $KT$
- B.  $R$
- C.  $VN$
- D.  $VB$
- E.  $VB_{max}$

**Questions 13-20.** In an orthogonal cutting operation using a coated carbide tool ( $n = 0.6$ ),  $t_o = 0.39 \text{ mm}$ ,  $V = 35 \text{ m/min}$ ,  $\alpha = 18^\circ$  and the  $w = 9 \text{ mm}$ . It is observed that  $t_c = 0.85 \text{ mm}$ ,  $F_c = 720 \text{ N}$  and  $F_t = 345 \text{ N}$ .

13. What is the value of the *chip-thickness ratio*?

- A. 2.18
- B. 0.33
- C. 3.02
- D. 0.46
- E. 1.0

14. What is the value of the *shear angle*?

- A.  $14.1^\circ$
- B.  $27.0^\circ$
- C.  $75.9^\circ$
- D.  $63.0^\circ$
- E.  $72.0^\circ$

15. What is the value of the *shear strain*?

- A. 1.96
- B. 0.67
- C. 2.12
- D. 1.16
- E. 0.16

16. What is the value of the *chip velocity*?

- A. 76.3 *m/min*
- B. 5.7 *m/min*
- C. 91.7 *m/min*
- D. 16.1 *m/min*
- E. 17.5 *m/min*

17. What is the magnitude of the *coefficient of friction*?

- A. 1.05
- B. 7.49
- C. 0.13
- D. 2.63
- E. 0.95

18. How much *energy* is required for 10 minutes of cutting?

- A. 25.2 *kJ*
- B. 252 *kJ*
- C. 43.2 *kJ*
- D. 0.72 *kJ*
- E. 1512 *kJ*

19. What is the effect on *tool life* of doubling the cutting speed?

- A. reduction in tool life by 50.0%
- B. reduction in tool life by 31.4%
- C. reduction in tool life by 66.0%
- D. reduction in tool life by 68.5%
- E. reduction in tool life by 34.0%

20. What is the effect on *material removal rate* of doubling the cutting speed?

- A. increase in the MRR by 50%
- B. decrease in the MRR by 50%
- C. doubling of the MRR
- D. increase in the MRR by 200%
- E. increase in the MRR by 150%

### Rules:

- You must prepare and submit the homework **individually**.
- Your work must be **neatly written** in pencil (or typed) and in **proper English** (where applicable).
- **Show all work**, and answer each question on a **separate sheet**.
- **BOX** your answer(s) and include the **units**.

Due date:

- **Sunday, May 04, 2014 (S2)**, 2014 (05/07/1435)
- **Monday, May 04, 2014 (S1,S3)**, 2014 (06/07/1435)

### Equations, Data, Diagrams You May Find Useful

$$\log x^p = p \log x, \quad \log xy = \log x + \log y, \quad \log \frac{x}{y} = \log x - \log y$$

$$\tan \phi = \frac{r \cos \alpha}{1 - r \sin \alpha} \Rightarrow r = \frac{t_0}{t_c} = \frac{\sin \phi}{\cos(\phi - \alpha)} \quad \alpha_e = \sin^{-1}(\sin^2 i + \cos^2 i \sin \alpha_n)$$

$$r = \frac{t_0}{t_c} = \frac{V_c}{V}$$

$$\gamma = \frac{AB}{OC} = \frac{AO}{OC} + \frac{OB}{OC} \Rightarrow \gamma = \cot \phi + \tan(\phi - \alpha)$$

Shear Stress =

$$\frac{F_s}{\text{Area of the shear plane}}$$

$$\frac{V}{\cos(\phi - \alpha)} = \frac{V_s}{\cos \alpha} = \frac{V_c}{\sin \phi}$$

$$\phi = 45^\circ + \frac{\alpha}{2} - \frac{\beta}{2} \quad (\text{when } \mu = 0.5 \sim 2)$$

$$\Rightarrow \phi = 45^\circ + \alpha - \beta$$

$$VT^n d^x f^y = C$$

$$T = C^{1/n} V^{-1/n} d^{-x/n} f^{-y/n}$$

$$T \approx C^7 V^{-7} d^{-1} f^{-4}$$

$$T = \frac{0.000665 Y_f}{\rho c} \sqrt[3]{\frac{V t_0}{K}}$$

$$\text{Power} = F_c V$$

$$\text{Power for friction} = F V_c$$

$$\text{Power for shearing} = F_s V_s$$

$$R_t = \frac{f^2}{8R}$$

$$T_{\text{mean}} \propto V^a f^b$$

- Carbide tools:  $a = 0.2, b = 0.125$
- High-speed steel tools:  $a = 0.5, b = 0.375$

$$u_t = u_s + u_f \quad u_s = \frac{F_s V_s}{w t_0 V}$$

$$u_f = \frac{F V_c}{w t_0 V} = \frac{F r}{w t_0}$$

$$\eta_{\text{mech}} = \frac{\text{Power}_c}{\text{Power}_{\text{source}}}$$

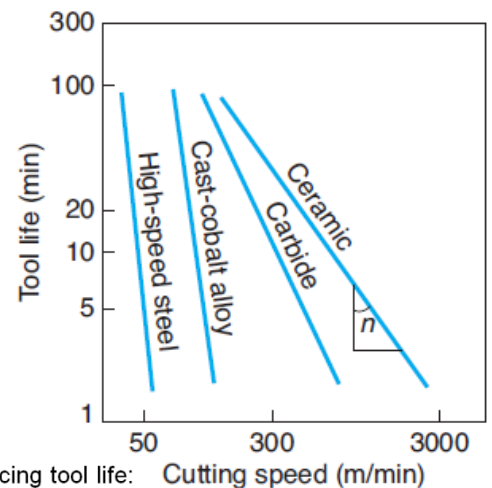
$$\mu = \frac{F}{N} = \frac{F_t + F_c \tan \alpha}{F_c - F_t \tan \alpha}$$

$$F_s = F_c \cos \phi - F_t \sin \phi$$

$$F_n = F_c \sin \phi + F_t \cos \phi$$

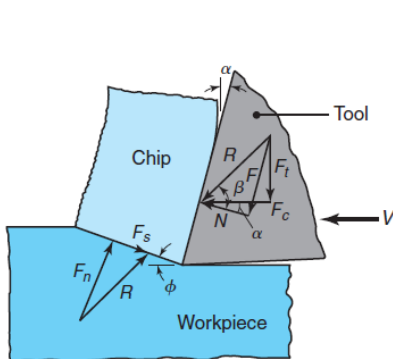
#### Ranges of n Values for the Taylor Equation (21.20a) for Various Tool Materials

High-speed steels	0.08–0.2
Cast alloys	0.1–0.15
Carbides	0.2–0.5
Coated carbides	0.4–0.6
Ceramics	0.5–0.7

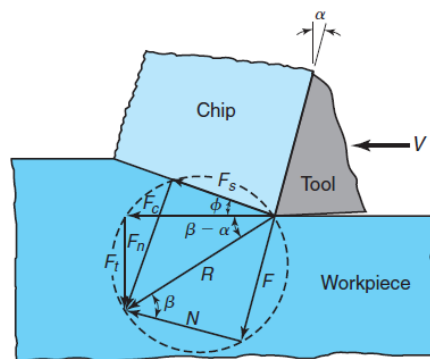


- Recommended cutting speed is one producing tool life:
  - 60-120 min: high-speed steel tools
  - 30-60 min: carbide tools

$$F_t = R \sin(\beta - \alpha) \quad \text{or} \quad F_t = F_c \tan(\beta - \alpha)$$



(a)



(b)

#### Approximate Range of Energy Requirements in Cutting Operations at the Drive Motor of the Machine Tool (for Dull Tools, Multiply by 1.25)

Material	Specific energy $W \cdot s/mm^3$
Aluminum alloys	0.4–1
Cast irons	1.1–5.4
Copper alloys	1.4–3.2
High-temperature alloys	3.2–8
Magnesium alloys	0.3–0.6
Nickel alloys	4.8–6.7
Refractory alloys	3–9
Stainless steels	2–5
Steels	2–9
Titanium alloys	2–5