

Problem 1:

1)

$$A_g = b * b , \quad A_s = 8 * \frac{\pi d_b^2}{4}$$

$$P_n = -A_s * f_y \Rightarrow -1277.25 * 10^3 = - \left(8 * \frac{\pi d_b^2}{4} \right) * 420$$

$$d_b = \sqrt{\frac{(-1277.25 * 10^3) * 4}{8 * 420 * \pi}} = 22 \text{ mm}$$

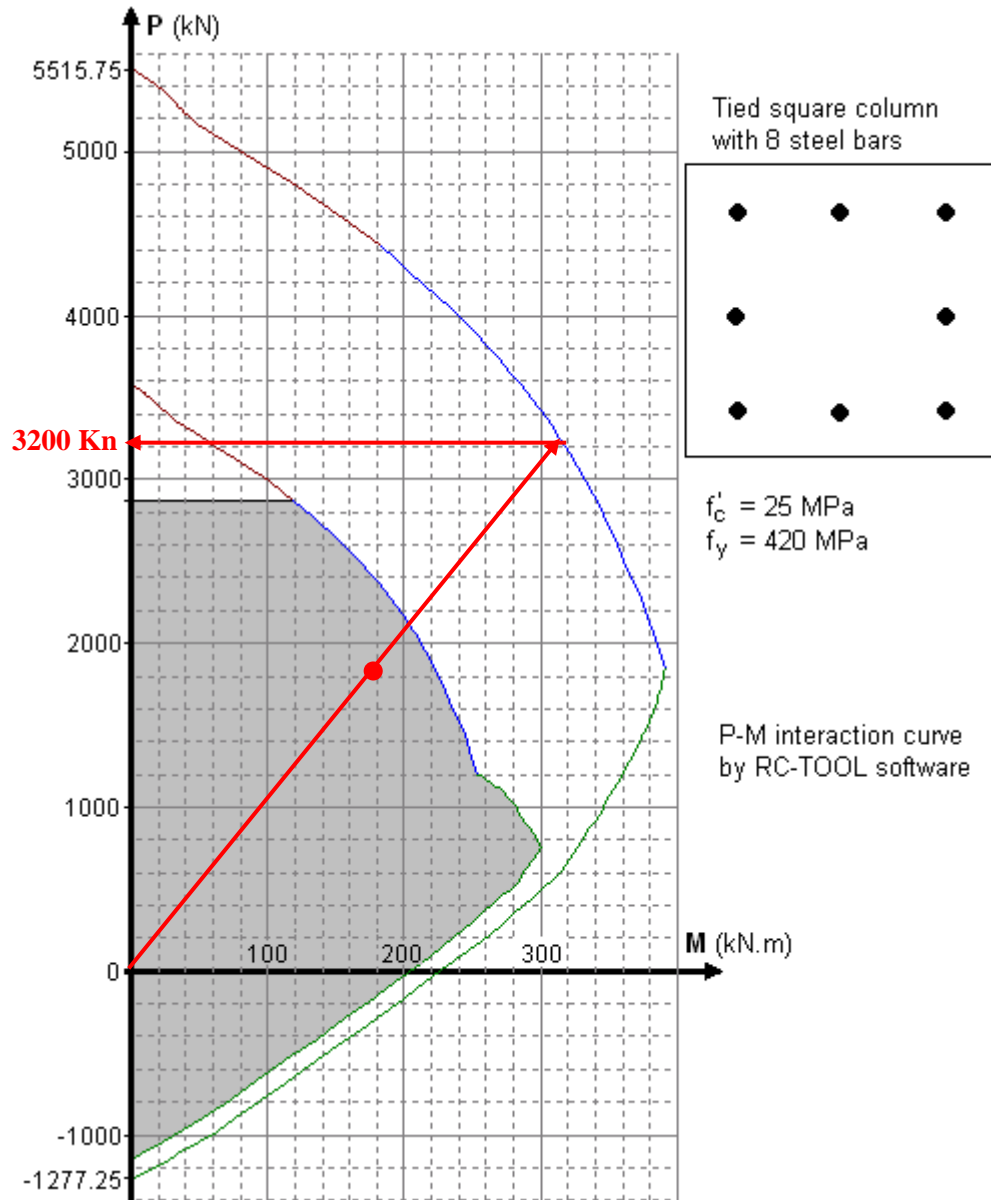
$$A_s = 8 * \frac{\pi * 22^2}{4} = 3039.52 \text{ mm}^2$$

$$P_o = [0.85 f_c (A_g - A_{st}) + f_y * A_{st}]$$

$$5515.75 * 10^3 = [0.85 * 25 * (A_g - 3039.52) + 420 * 3039.52]$$

$$A_g = \frac{4303741.4}{21.25} = 202529.007 \text{ mm}^2$$

$$b = \sqrt{202529.007} = 450 \text{ mm}$$



Bresler reciprocal method :-

All points are located in shaded area (safe zone)

$$P_o = 5515.75 \text{ Kn}$$

$$\frac{1}{P_n} = \frac{1}{P_{nx}} + \frac{1}{P_{ny}} - \frac{1}{P_{no}} = \frac{1}{3200} + \frac{1}{3200} - \frac{1}{5515.75} = 4.437 * 10^{-4} \text{ 1/Kn}$$

$$P_n = 2253.77 \text{ Kn} \Rightarrow \phi P_n = 0.65 * 2253.77 = 1464.95 \text{ Kn} < P_u$$

The column is not safe

3)

$$f'_c = 25 \text{ MPa} \quad , \quad 350 \times 350 \quad , \quad L = 4700 \quad , \quad P_u = 1800 \text{ Kn}$$

$$K = 1 \quad , \quad M_1 = 80 \text{ Kn.m} \quad , \quad M_2 = 180 \text{ Kn.m}$$

Clockwise moment → Double curvature

$$\frac{1 * 4700}{0.3 * 350} \leq 34 - 12 \left(\frac{80}{-180} \right) \Rightarrow 44.762 \not\leq 39.33$$

⇒ slender column (Long column)

$$C_m = 0.6 + 0.4 \left(\frac{80}{-180} \right) \geq 0.4$$

$$C_m = 0.422$$

$$I_g = \frac{b * h^3}{12} = \frac{350 * 350^3}{12} = 1.2505 \times 10^9 \text{ mm}^4$$

$$E_c = 4700 \sqrt{f'_c} = 4700 \sqrt{25} = 23500 \text{ Mpa}$$

$$\beta_d = 0.6$$

$$EI = \frac{0.4 * E_c * I_g}{1 + \beta_d} = \frac{0.4 * 23500 * 1.2505 \times 10^9}{1 + 0.6} = 7.3468 \times 10^{12} \text{ N.mm}^2$$

$$P_c = \frac{\pi^2 EI}{(kL_u)^2} = \frac{\pi^2 (7.3468 \times 10^{12})}{(1 * 4700)^2} * 10^{-3} = 3279.1583 \text{ Kn}$$

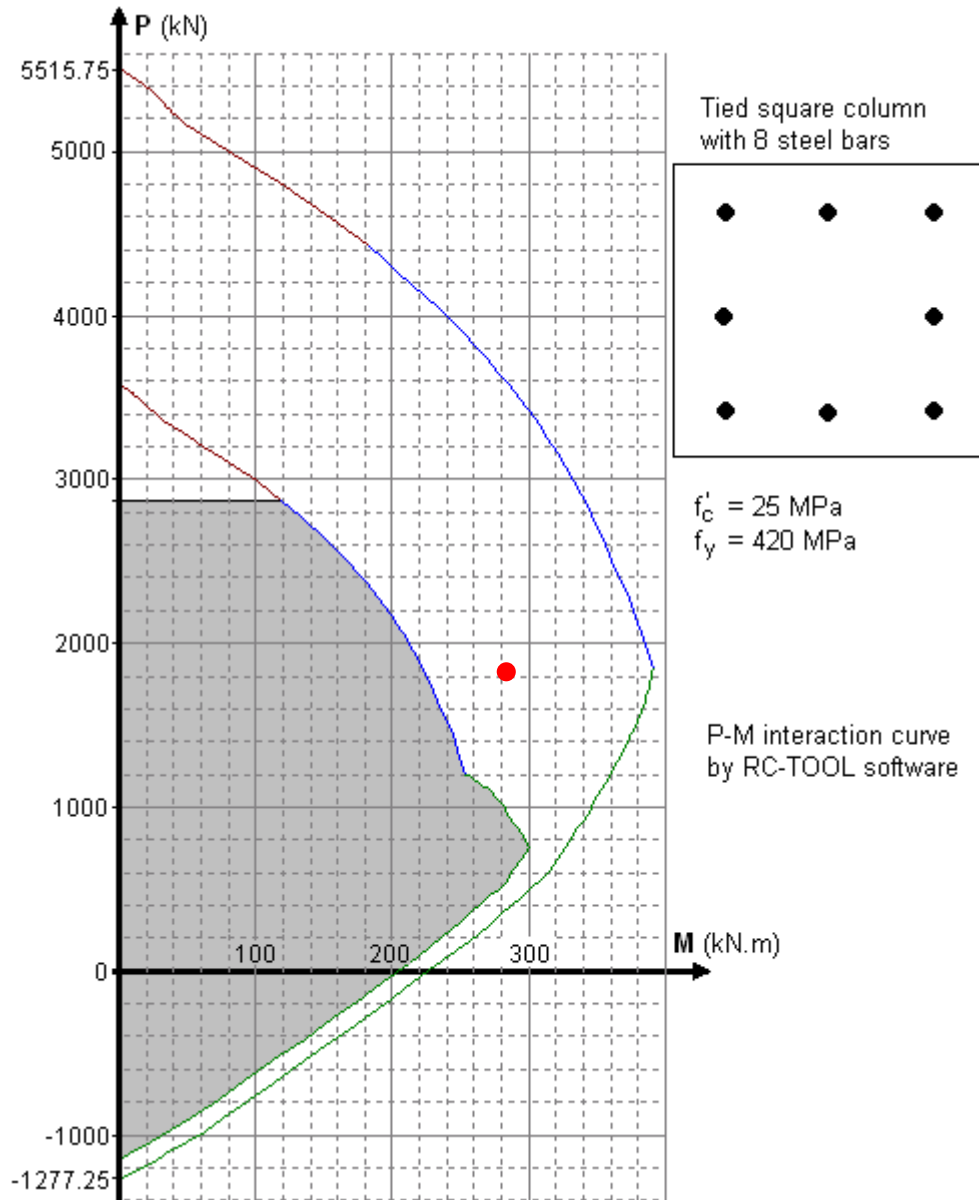
$$M_{2_{\min}} = p_u * (15 + 0.03h) = 1800 * (15 + 0.03 * 350) 10^{-3} = 45.9 \text{ Kn.m}$$

$$M_2 = \max(M_2, M_{2_{\min}}) = 180 \text{ Kn.m}$$

$$\delta_{ns} = \frac{C_m}{1 - \frac{P_u}{0.75 * P_c}} \geq 1 \Rightarrow \frac{0.422}{1 - \frac{1800}{0.75 * 3279.1583}} = 1.575$$

$$\therefore \delta_{ns} = 1.575$$

$$M_c = \delta_{ns} * M_2 = 1.575 * 180 = 283.5 \text{ Kn.m}$$



This point (1800, 283.5) is located in unsafe zone ... OK the column is not safe

Problem 2:

1)

$$Wu = 1.4(2.5 + 0.2 * 24) + 1.7(2.5) = 14.47 \text{ Kn/m}^2$$

1) Exterior panel

$$L_n = 6 - \frac{0.3}{2} - \frac{0.3}{2} = 5.7 \text{ m}$$

$$h_{min} = \frac{L_n}{30} = \frac{5700}{30} = 190 \text{ mm}$$

2) Interior panel

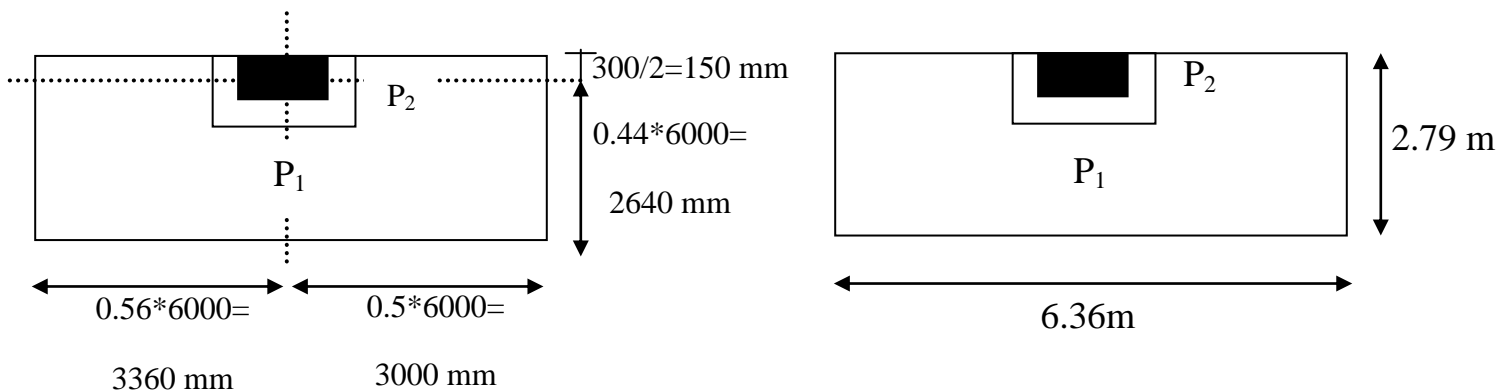
$$L_n = 6 - \frac{0.3}{2} - \frac{0.3}{2} = 5.7 \text{ m}$$

$$h_{min} = \frac{L_n}{33} = \frac{5700}{33} = 172.73 \text{ mm}$$

$$h_{min} = \text{Max}(190, 172.73) = 190 \text{ mm}$$

$$h > h_{min} \rightarrow \text{ok}$$

2)



$$P_1 = C_1 + d_{ave} = 300 + 168 = 468 \text{ mm}$$

$$P_2 = C_2 + \frac{d_{ave}}{2} = 300 + \frac{168}{2} = 384 \text{ mm}$$

$$V_u = W_u(A_o - A_c) = 14.47(6.36 * 2.79 - 0.468 * 0.384) = 254.16 \text{ KN}$$

$$b_o = \text{length of critical perimeter} = (P_1 + 2 * P_2) = (468 + 2 * 384) = 1236 \text{ mm.}$$

$$\beta_c = \text{column length ratio} \left(\frac{\text{long side}}{\text{short side}} \right) = \frac{300}{300} = 1$$

$$\alpha_s = 30$$

$$V_c = \text{Min} \left\{ \begin{array}{l} \left(1 + \frac{2}{1}\right) \frac{\sqrt{25}}{6} * 1236 * 168 * 10^{-3} = 519.12 \text{ Kn} \\ \left(2 + \frac{30 * 168}{1236}\right) \frac{\sqrt{25}}{12} * 1320 * 168 * 10^{-3} = 525.84 \text{ KN} \\ \frac{\sqrt{25}}{3} * 1236 * 168 * 10^{-3} = 346.08 \text{ Kn} \end{array} \right\}$$

$$= 346.08 \text{ KN}$$

$$\phi V_c = 0.75 * 346.08 = 259.56 \text{ Kn} > 254.16 \text{ Kn} \therefore \text{two way shear is ok}$$

3)

	Span B ₁ -B ₂		
L₁ (m)	6		
L₂ (m)	6		
L_n (m)	5.7		
$M_o = W_s L_2 \frac{L_n^2}{8}$ (KN.m)	352.59		
L_{min} (m)	6		
CS width (m) = 0.5 L_{min}	3		
Moment coefficients	0.26	0.52	0.7
-ve and +ve moments	91.68	183.34	246.82
CS moment (%)	100	60	75
CS moments (kN.m)	91.68	110.01	185.11
MS moment (%)	0	40	25
MS moments (kN.m)	0	73.34	61.71

4)

$$b = 3000 \text{ mm} \quad , \quad M_u = 180 \text{ kn.m}$$

$$d = 174 \text{ mm} \quad , \quad R_n = \frac{180/0.9}{3000 * 174^2} * 10^6 = 2.20 \text{ Mpa}$$

$$m = \frac{420}{0.85 * 25} = 19.765 \quad ,$$

$$\rho = \frac{1}{19.765} \left(1 - \sqrt{1 - \frac{2 * 2.20 * 19.765}{420}} \right) = 0.00555$$

$$A_s = 0.00555 * 3000 * 174 = 2895.45 \text{ mm}^2 \quad ,$$

$$A_{s \text{ min}} = 0.0018 * 3000 * 200 = 1080 \text{ mm}^2$$

$$S_{max} = \min \left(\frac{113.04}{2895.4} * 3000 = 117.12 \text{ mm}, 300 \text{ mm}, 2 * 200 = 400 \right) \\ = 117.12 \text{ mm}$$

for flexural \rightarrow use $\emptyset 12 @ 115 \text{ mm}$

5)

$$0.2 < \alpha = 1.9 < 2$$

$$\beta = \frac{6000 - 300}{6000 - 300} = 1$$

$$h_{min} = \frac{L_n \left(0.8 + \frac{f_y}{1500} \right)}{36 + 9\beta(\alpha_m - 0.2)}$$

$$h_{min} = \frac{5700 \left(0.8 + \frac{420}{1500} \right)}{36 + 5 * 1(1.9 - 0.2)} = 138.34 \text{ mm}$$

$$h = 145 > h_{min} \quad \text{thickness is ok}$$