

Bond and Development Length:

$$l_d = \max \left\{ \begin{array}{l} \text{detailed or simplified equation} \\ 300 \text{ mm} \end{array} \right. \quad \rightarrow \text{straight Development length, SBC - 18, 25.4.2.1}$$

$$l_d = \begin{cases} \left[\frac{f_y \Psi_t \Psi_e}{2.1 \lambda \sqrt{f'_c}} \right] d_b & d_b \leq 20 \\ \left[\frac{f_y \Psi_t \Psi_e}{1.7 \lambda \sqrt{f'_c}} \right] d_b & d_b \geq 22 \end{cases} \quad \rightarrow \text{simplified equation, SBC - 18, 25.4.2.2}$$

$$l_d = \left[\frac{f_y}{1.1 \lambda \sqrt{f'_c}} \frac{\Psi_t \Psi_e \Psi_s}{\left(\frac{c_b + K_{tr}}{d_b} \right)} \right] d_b \quad \rightarrow \text{detailed equation, SBC - 18, 25.4.2.3}$$

$$\frac{c_b + K_{tr}}{d_b} \leq 2.5 \quad \rightarrow \text{requirement, SBC - 18, 25.4.2.3}$$

$$K_{tr} = \frac{40A_{tr}}{sn} \quad \rightarrow \text{transverse reinforcement index, mm}$$

$$c_b = \min \left\{ \begin{array}{l} \text{distance to bar centroid} \\ \frac{1}{2} \text{ center to center bar spacing} \end{array} \right.$$

$$\text{distance to bar centroid} = \text{cover} + d_s + \frac{d_b}{2}$$

$$\frac{1}{2} \text{ center to center bar spacing} = \frac{1}{2} \left(\frac{b - 2\text{cover} - 2d_s - d_b}{n - 1} \right)$$

$$\lambda = \begin{cases} 0.75 & \text{lightweight concrete} \\ 1.0 & \text{normal concrete} \end{cases} \quad \rightarrow \text{concrete weight factor, SBC - 18, Table 25.4.2.4}$$

$$\Psi_e = \begin{cases} 1.5 & \text{coated, } c < 3d_b \text{ or } s < 6d_b \\ 1.2 & \text{coated, other conditions} \\ 1.0 & \text{uncoated} \end{cases} \quad \rightarrow \text{coating factor, SBC - 18, Table 25.4.2.4}$$

$$\Psi_s = \begin{cases} 0.8 & d_b \leq 20 \\ 1.0 & d_b \geq 22 \end{cases} \quad \rightarrow \text{reinforcement size factor, SBC - 18, Table 25.4.2.4}$$

$$\Psi_t = \begin{cases} 1.3 & \text{top bars} \\ 1.0 & \text{bottom bars} \end{cases} \quad \rightarrow \text{reinforcement location factor, SBC - 18, Table 25.4.2.4}$$

$l_{dh} = \max \begin{cases} \text{equation} \\ 8d_b \\ 150 \text{ mm} \end{cases}$
→ Development of standard hooks, SBC – 18, 25.4.3.1

$l_{dh} = \left(\frac{0.24 f_y \Psi_e \Psi_c \Psi_r}{\lambda \sqrt{f'_c}} \right) d_b$
→ Development of standard hooks, SBC – 18, 25.4.3.1

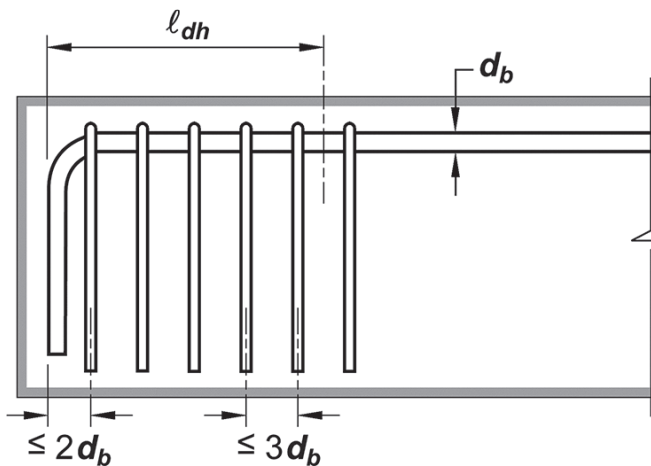
$\lambda = \begin{cases} 0.75 & \text{lightweight concrete} \\ 1.0 & \text{normal concrete} \end{cases}$
→ concrete weight factor, SBC – 18, Table 25.4.3.2

$\Psi_e = \begin{cases} 1.2 & \text{coated} \\ 1.0 & \text{uncoated} \end{cases}$
→ coating factor, SBC – 18, Table 25.4.3.2

$\Psi_c = \begin{cases} 0.7 & d_b \leq 36, \text{ side cover} \geq 65, \text{ end cover} \geq 50 \\ 1.0 & \text{other} \end{cases}$
→ cover factor, SBC – 18, Table 25.4.3.2

$\Psi_r = \begin{cases} 0.8 & \text{see figure} \\ 1.0 & \text{other} \end{cases}$
→ confining reinforcement factor, SBC – 18, Table 25.4.3.2

enclosed along l_{dh} within stirrups perpendicular to l_{dh} at $s \leq 3d_b$,



enclosed along the bar extension beyond hook including the bend within stirrups perpendicular to l_{ext} at $s \leq 3d_b$

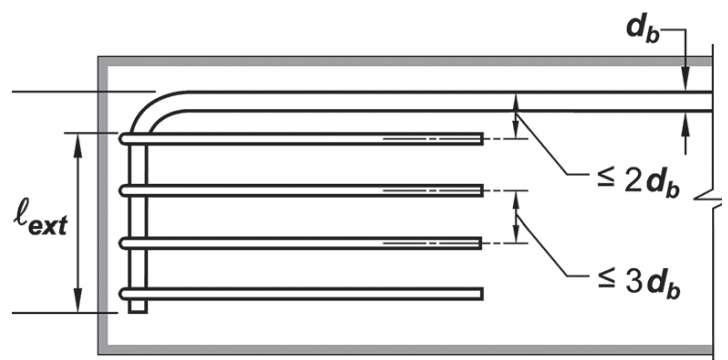
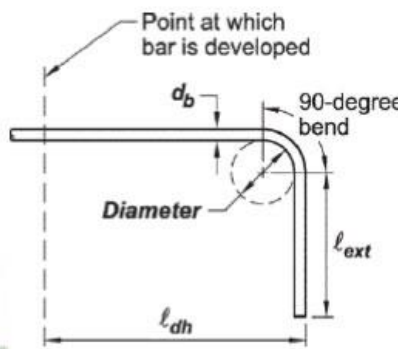
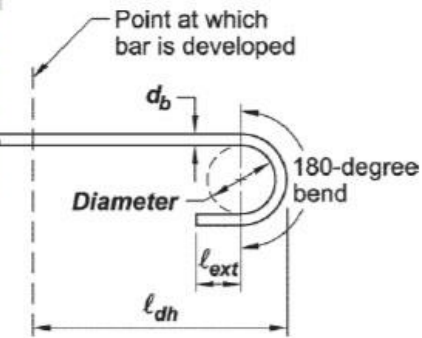
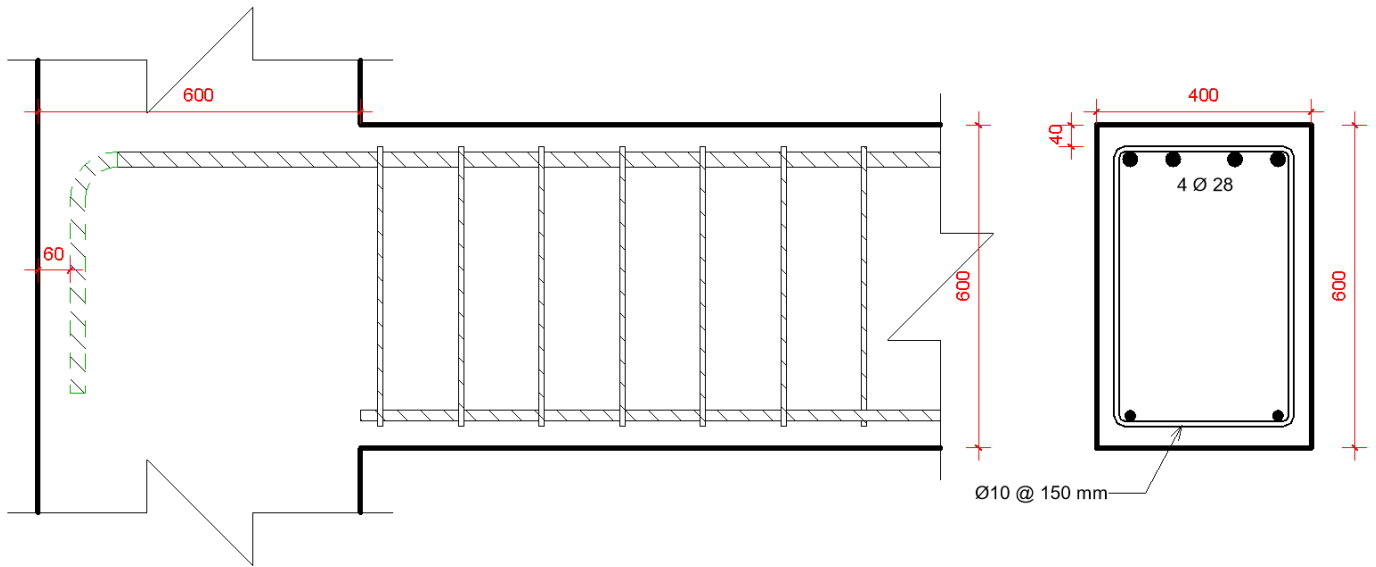


Table 25.3.1—Standard hook geometry for development of deformed bars in tension

Type of standard hook	Bar size	Minimum inside bend diameter, mm	Straight extension ^[1] l_{ext} , mm	Type of standard hook
90-degree hook	Dia 10 through Dia 25	$6d_b$	$12d_b$	
	Dia 28 through Dia 36	$8d_b$		
	Dia 45 and Dia 60	$10d_b$		
180-degree hook	Dia 10 through Dia 25	$6d_b$	Greater of $4d_b$ and 65 mm	
	Dia 28 through Dia 36	$8d_b$		
	Dia 45 and Dia 60	$10d_b$		



A 400×600 mm cantilever beam, reinforced by 4Ø28, is supported by a 400×600 mm column.

a) Calculate the required straight development length using the detailed equation assuming $K_{tr} = 0$, $f'_c = 35$ MPa, $f_y = 420$ MPa.

b) Is the width of the column sufficient to develop the bars straight? If not, design the suitable standard hook for the beam-column joint and draw the reinforcement details.

a)

$\lambda = 1.0$ normal weight concrete

$\Psi_t = 1.3$ top bars

$\Psi_e = 1.0$ uncoated

$\Psi_s = 1.0$ $d_b = 28 \geq 22$

$K_{tr} = 0$ given

$$c_b = \min \left\{ \begin{array}{l} \text{distance to bar centroid} = \text{cover} + d_s + \frac{d_b}{2} = 40 + 10 + 14 = 64 \text{ mm} \\ \frac{1}{2} \text{ center to center bar spacing} = \frac{1}{2} \left(\frac{400 - 2 \times 40 - 2 \times 10 - 28}{4 - 1} \right) = 45.33 \text{ mm} \end{array} \right.$$

$$c_b = 45.33 \text{ mm}$$

$$\frac{c_b + K_{tr}}{d_b} = \frac{45.33 + 0}{28} = 1.62 \leq 2.5 \rightarrow OK$$

$$l_d = \left[\frac{f_y}{1.1\lambda\sqrt{f'_c}} \frac{\Psi_t \Psi_e \Psi_s}{\left(\frac{c_b + K_{tr}}{d_b} \right)} \right] d_b = \left[\frac{420}{1.1 \times 1.0 \times \sqrt{35}} \frac{1.3 \times 1.0 \times 1.0}{1.62} \right] d_b$$

$$l_d = 51.27d_b = 51.27 \times 28 = 1435.6 \text{ mm}$$

b) $l_d = 1435.6$ mm is larger than the column dimensions (600 mm), standard hook should be used.

$$\lambda = 1.0 \quad \text{normal concrete}$$

$$\Psi_e = 1.0 \quad \text{uncoated}$$

$$\Psi_c = 1.0 \quad d_b = 28 \leq 36, \text{ side cover} = 40 \leq 65, \text{ end cover} = 60 \geq 50$$

$$\Psi_r = 1.0 \quad \text{assumed since no available information}$$

$$l_{dh} = \left(\frac{0.24 \times 420 \times 1.0 \times 1.0 \times 1.0}{1.0 \times \sqrt{35}} \right) d_b = 17.04 d_b = 17.04 \times 28 = 477.07 \text{ mm}$$

Room available for hook development = column dimension – end cover = 600 – 60 = 540 mm

Hook development length = 477.07 mm < available room = 540 mm → OK

Check if 90° hook can be used.

- Minimum inside bend diameter from SBC304-18, Table 25.3.1 = $8d_b = 224$ mm
- Minimum straight extension l_{ext} from SBC304-18, Table 25.3.1 = $12d_b = 336$ mm
- Total required hook tail height = bend dia/2 + l_{ext} + $d_b = 224/2 + 336 + 28 = 476$ mm
- Available room for hook tail = h – 2 clear covers = 600 - 2×50 = 500 mm

Available room = 500 mm > required hook tail height = 476 mm → 90° hook can be used.

Actually, since the bars are developed into a column, it can be used. That is because a column has greater depth than the beam.

Check if 180° hook can be used.

- Minimum inside bend diameter from SBC304-18, Table 25.3.1 = $8d_b = 224$ mm
- Minimum straight extension l_{ext} from SBC304-18, Table 25.3.1 = $4d_b = 112$ mm > 65 mm
- Total required hook tail height = bend dia + $2d_b = 224 + 2 \times 28 = 280$ mm
- Available room for hook tail = h – 2 clear covers = 600 - 2×50 = 500 mm

Available room = 500 mm > required hook tail height = 280 mm → Use 180° hook.

