

## Shear Analysis and Design in Beams:

$$V_n = V_c + V_s \quad \rightarrow \text{Nominal shear strength in beams, SBC – 18, 22.5.1.1}$$

$$V_c = \left( \frac{\sqrt{f'_c}}{6} \right) b_w d \quad \rightarrow \text{shear strength carried by Concrete}$$

$$V_s = \frac{A_v f_{yt} d}{s} \quad \rightarrow \text{shear strength carried by steel, SBC – 18, 22.5.10.5.3}$$

$$V_{s \max} = \frac{2}{3} \sqrt{f'_c} b_w d = 4V_c \quad \rightarrow \text{max. shear strength resisted by steel, SBC – 18, 22.5.1.2}$$

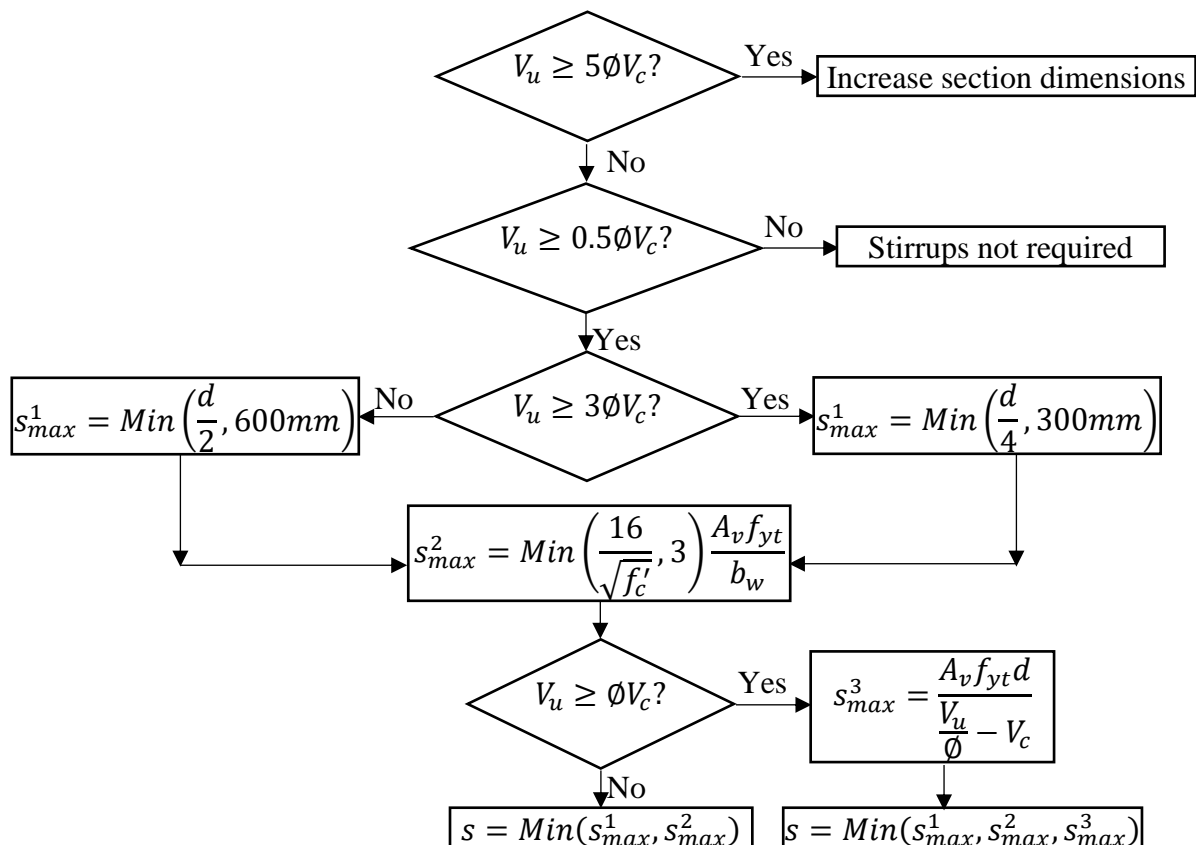
$$\phi = 0.75 \quad \rightarrow \text{shear strength reduction factor, SBC – Table 21.2.1}$$

$$\phi V_e = w_u \frac{l_n}{2} \quad \rightarrow \text{shear force at the end of beam (simply supported beam)}$$

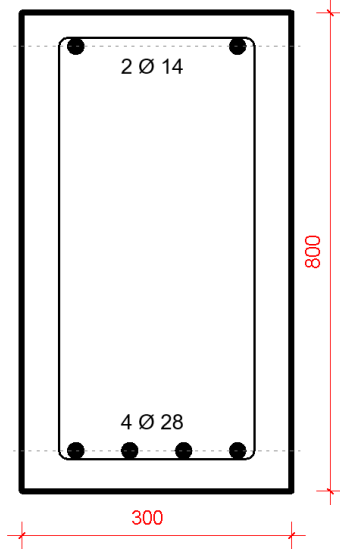
$$\phi V_m = w_{uL} \frac{l_n}{8} \quad \rightarrow \text{shear force at the middle of beam (simply supported beam)}$$

$$\left( \frac{V_u}{\phi} \right)_x = V_e - \frac{2x}{l_n} (V_e - V_m) \quad \rightarrow \frac{V_u}{\phi} \text{ at distance } x \text{ from the face of supports}$$

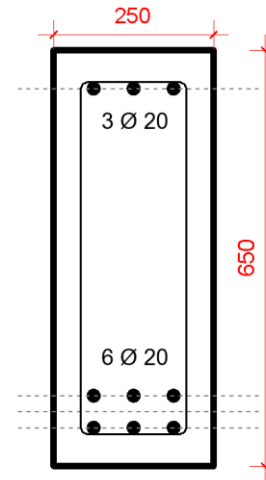
$$x = \frac{(V_e - \frac{V_u}{\phi})}{V_e - V_m} \times \frac{l_n}{2} \quad \rightarrow \text{distance } x \text{ from the face of supports where } \frac{V_u}{\phi} \text{ occurs}$$



Beam A:  
Ø 8 stirrups @ 250 mm



Beam B:  
Ø 12 stirrups @ 100 mm



Which section is sufficient to resist ultimate shear stress of 300 kN?  $f'_c = 30 \text{ MPa}$ ,  $f_y = 420 \text{ MPa}$ ,  $S_l=30$

Beam: A.

1- Find,  $d$ .

$$d = h - \text{cover} - d_s - \frac{d_b}{2} = 800 - 40 - 8 - 14 = 738 \text{ mm}$$

2- Find  $V_c$ :

$$V_c = \left( \frac{\sqrt{f'_c}}{6} \right) b_w d = \left( \frac{\sqrt{30}}{6} \right) 300 \times 738 = 202109.6 \text{ N}$$

3- Find  $V_s$ :

$$A_v = 2 \times \pi \frac{8^2}{4} = 100.53 \text{ mm}^2$$

$$V_s = \frac{A_v f_{yt} d}{s} = \frac{100.53 \times 420 \times 738}{250} = 124641.1 \text{ N}$$

3- Find  $\phi V_n$ :

$$V_n = V_c + V_s = 202109.6 + 124641.1 = 326750.7 \text{ N}$$

$$\phi V_n = 0.75 \times 326.75 = 245.06 \text{ kN}$$

$$\phi V_n = 245.06 < V_u = 300$$

This beam cannot resist the existing shear stress.

Beam: B.

1- Find,  $d$ .

$$d_t = h - \text{cover} - d_s - \frac{d_b}{2} = 650 - 40 - 10 - 10 = 590 \text{ mm}$$

$$d_{min} = d_1 - S - d_b = 590 - 30 - 20 = 540 \text{ mm}$$

$$d = (d_t + d_{min})/2 = 565 \text{ mm}$$

2- Find  $V_c$ :

$$V_c = \left( \frac{\sqrt{f'_c}}{6} \right) b_w d = \left( \frac{\sqrt{30}}{6} \right) 250 \times 565 = 128943 \text{ N}$$

3- Find  $V_s$ :

$$A_v = 2 \times \pi \frac{12^2}{4} = 157.08 \text{ mm}^2$$

$$V_s = \frac{A_v f_{yt} d}{s} = \frac{157.08 \times 420 \times 565}{100} = 372750 \text{ N}$$

3- Find  $\phi V_n$ :

$$V_n = V_c + V_s = 128943 + 372750 = 501693 \text{ N}$$

$$\phi V_n = 0.75 \times 501.693 = 376.27 \text{ kN}$$

$$\phi V_n = 376.27 > V_u = 300$$

This beam can resist the existing shear stress

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Design for shear a simply supported beam with 8-m clear span and the rectangular section of 850×400 mm, subjected to uniform loading including dead load of 45 kN/m and live load of 32 kN/m. Use two-legged 10 mm stirrups and steel depth  $d = 758$  mm.

Determine the stirrup spacing at the critical section (as a multiple of 50 mm) and the stirrup distribution using a second spacing value 50 mm greater than the first one.  $f'_c = 20$  MPa,  $f_y = 420$  MPa,  $d_s = 10$  mm,  $S_l = 28$  mm.

1- Find factored shear force at end and middle of the span,  $V_e$  and  $V_m$  and  $V_u/\phi$  at distance  $d$  from support.

$$w_u = 1.4DL + 1.7LL = 1.4 \times 45 + 1.7 \times 32 = 117.4 \text{ kN/m}$$

$$w_{uL} = 1.7LL = 1.7 \times 32 = 54.4 \text{ kN/m}$$

$$\phi V_e = w_u \frac{l_n}{2} = 117.4 \times \frac{8}{2} = 469.6 \text{ kN}$$

$$V_e = \frac{469.6}{0.75} = 626.13 \text{ kN}$$

$$\phi V_m = w_{uL} \frac{l_n}{8} = 54.4 \times \frac{8}{8} = 54.4 \text{ kN}$$

$$V_m = \frac{54.4}{0.75} = 72.53 \text{ kN}$$

$$\left(\frac{V_u}{\phi}\right)_x = V_e - \frac{2x}{l_n}(V_e - V_m) = 626.13 - \frac{2 \times 758}{8000}(626.13 - 72.53) = 521.226 \text{ kN} = 521226 \text{ N}$$

2- Check beam dimensions adequacy and if stirrups are required.

$$V_c = \left(\frac{\sqrt{f'_c}}{6}\right) b_w d = \left(\frac{\sqrt{20}}{6}\right) 400 \times 758 = 225992 \text{ N}$$

$$5\phi V_c = 5 \times 0.75 \times 225.992 = 847.47 \text{ kN} > V_u = 521.23 \text{ kN}$$

$V_u < 5\phi V_c \rightarrow$  section dimensions are satisfactory.

$$0.5\phi V_c = 0.5 \times 0.75 \times 225.992 = 84.747 \text{ kN} < V_u = 521.23 \text{ kN}$$

$V_u > 0.5\phi V_c \rightarrow$  stirrups are required, calculate  $A_v$

$$A_v = 2 \times \pi \frac{d_s^2}{4} = 2 \times \pi \frac{10^2}{4} = 157.08 \text{ mm}^2$$

3- Find maximum spacings,  $S^1_{max}$ ,  $S^2_{max}$  and  $S^3_{max}$

$$3\phi V_c = 3 \times 0.75 \times 225.992 = 508.482 \text{ kN} < V_u = 521.23 \text{ kN}$$

$$3\phi V_c < V_u \rightarrow s^1_{max} = \text{Min}\left(\frac{d}{4}, 300\text{mm}\right) = 189.5 \text{ mm}$$

$$s^2_{max} = \text{Min}\left(\frac{16}{\sqrt{f'_c}}, 3\right) \frac{A_v f_{yt}}{b_w} = \text{Min}\left(\frac{16}{\sqrt{20}}, 3\right) \frac{157.08 \times 420}{400} = 494.8 \text{ mm}$$

$$s^3_{max} = \frac{A_v f_{yt} d}{\frac{V_u}{\phi} - V_c} = \frac{157.08 \times 420 \times 758}{\frac{521226}{0.75} - 225992} = 106.6 \text{ mm}$$

$$s = \text{Min}(s_{max}^1, s_{max}^2, s_{max}^3) = 106.6 \text{ mm}$$

Use  $s = 100 \text{ mm}$  at critical section.

4- Find spacing at other sections.

First spacing  $s_1 = 100 \text{ mm} \rightarrow$  Second spacing  $s_2 = 150 \text{ mm} \rightarrow$  Third spacing  $s_3 = 200 \text{ mm}, \dots$  so on.

@ First spacing:

$$s_1 = 100 \text{ mm} @ V_u = 521.226 \text{ kN}$$

@ Second spacing:

$$V_n = V_c + V_s = V_c + \frac{A_v f_{yt} d}{s} = 225992 + \frac{157.08 \times 420 \times 758}{150} = 559378 \text{ N} = 559.378 \text{ kN}$$

$$x = \frac{\left(V_e - \frac{V_u}{\phi}\right)}{V_e - V_m} \times \frac{l_n}{2} = \frac{(626.13 - 559.378)}{626.13 - 72.53} \times \frac{8}{2} = 0.482 \text{ m}$$

@ Third spacing:

$$V_n = V_c + V_s = V_c + \frac{A_v f_{yt} d}{s} = 225992 + \frac{157.08 \times 420 \times 758}{200} = 476031 \text{ N} = 476.031 \text{ kN}$$

$$x = \frac{\left(V_e - \frac{V_u}{\phi}\right)}{V_e - V_m} \times \frac{l_n}{2} = \frac{(626.13 - 476.031)}{626.13 - 72.53} \times \frac{8}{2} = 1.085 \text{ m}$$

@ Forth spacing:

$$V_n = V_c + V_s = V_c + \frac{A_v f_{yt} d}{s} = 225992 + \frac{157.08 \times 420 \times 758}{250} = 426023 \text{ N} = 426.023 \text{ kN}$$

$$x = \frac{\left(V_e - \frac{V_u}{\phi}\right)}{V_e - V_m} \times \frac{l_n}{2} = \frac{(626.13 - 426.023)}{626.13 - 72.53} \times \frac{8}{2} = 1.446 \text{ m}$$

@ No stirrups required:

$$\frac{V_u}{\phi} = V_n = 0.5\phi V_c = 0.5 \times 225992 = 112996 \text{ N} = 112.966 \text{ kN}$$

$$x = \frac{\left(V_e - \frac{V_u}{\phi}\right)}{V_e - V_m} \times \frac{l_n}{2} = \frac{(626.13 - 112.966)}{626.13 - 72.53} \times \frac{8}{2} = 3.708 \text{ m}$$

5- find number of stirrups.

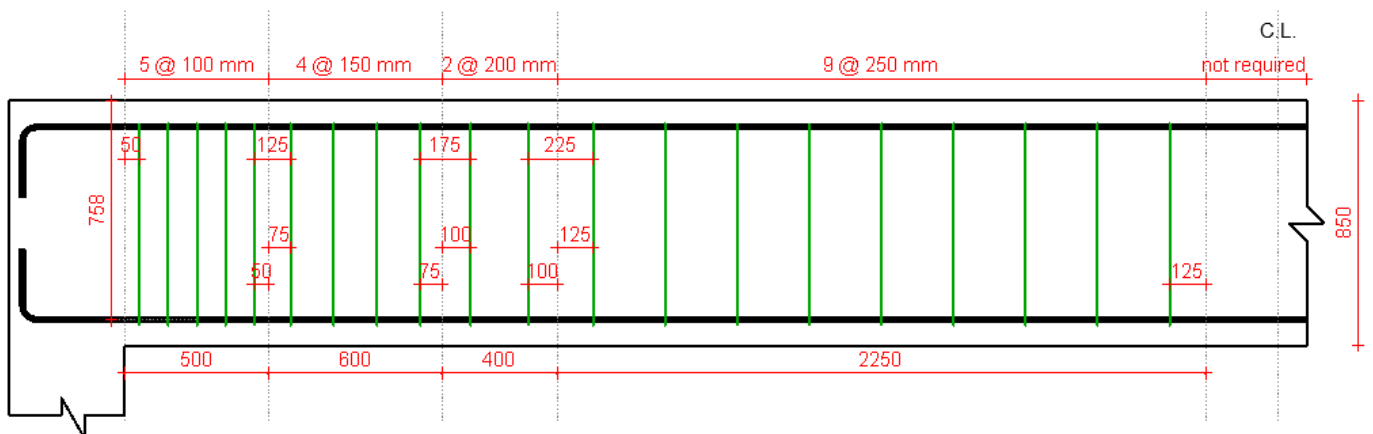
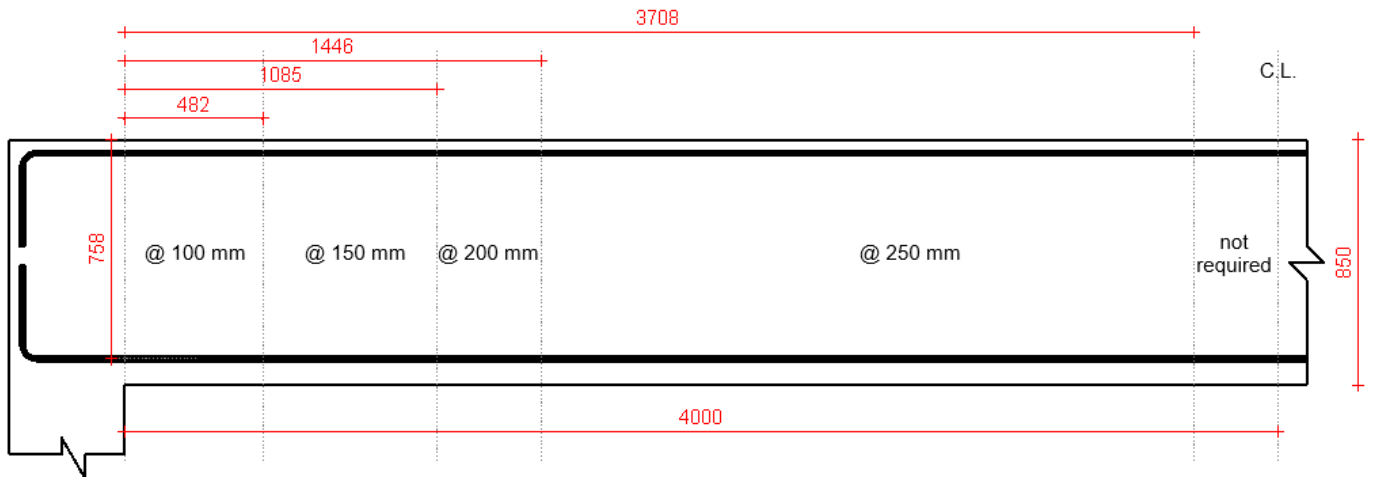
$$\text{Number of stirrups} = \frac{\text{Distance in which stirrups of the same spacing has to be provided}}{\text{spacing between the stirrups}}$$

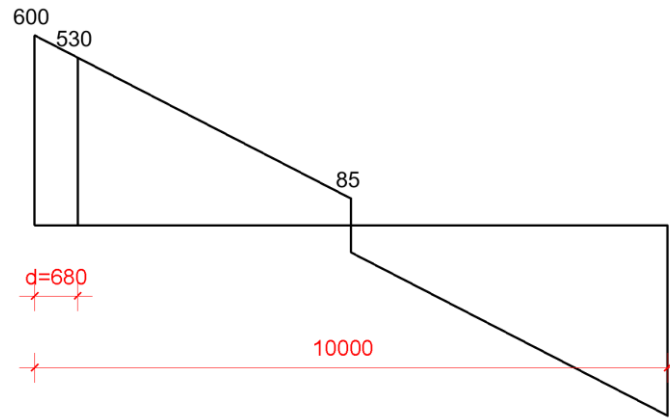
$$(\text{Number of stirrups})_{s=100} = \frac{482 - 50}{100} = 4.32 \text{ use } 5@100 \text{ mm}$$

$$(\text{Number of stirrups})_{s=150} = \frac{1085 - (50 + 5 \times 100)}{150} = 3.56 \text{ use } 4@150 \text{ mm}$$

$$(\text{Number of stirrups})_{s=200} = \frac{1446 - (50 + 5 \times 100 + 4 \times 150)}{200} = 1.48 \text{ use } 2@200 \text{ mm}$$

$$(\text{Number of stirrups})_{s=250} = \frac{3708 - (50 + 5 \times 100 + 4 \times 150 + 2 \times 200)}{250} = 8.63 \text{ use } 9@250 \text{ mm}$$





Using the shear force envelope given ( $V_u/\phi$ ), (a) check that the section is large enough ( $800 \times 500$  mm) for shear design and (b) determine the required spacing of stirrups to resist maximum ultimate shear at the shear critical section of the girder (use  $\phi 12$  stirrups).  $f'_c = 28$  MPa,  $f_y = 420$ .

(a)

$$V_c = \left( \frac{\sqrt{f'_c}}{6} \right) b_w d = \left( \frac{\sqrt{28}}{6} \right) 500 \times 680 = 299852 \text{ N} = 299.852 \text{ kN}$$

$$5V_c = 5 \times 299.852 = 1499.26 \text{ kN} > V_u = 530 \text{ kN}$$

$V_u < 5\phi V_c \rightarrow$  section dimensions are satisfactory.

(b)

Find maximum spacings,  $s^1_{max}$ ,  $s^2_{max}$  and  $s^3_{max}$

$$A_v = 2 \times \pi \frac{d_s^2}{4} = 2 \times \pi \frac{12^2}{4} = 226.1 \text{ mm}^2$$

$$3\phi V_c = 3 \times 0.75 \times 299.852 = 674.667 \text{ kN} > V_u = 530 \text{ kN}$$

$$3\phi V_c > V_u \rightarrow s^1_{max} = \text{Min} \left( \frac{d}{2}, 600 \text{ mm} \right) = 340 \text{ mm}$$

$$s^2_{max} = \text{Min} \left( \frac{16}{\sqrt{f'_c}}, 3 \right) \frac{A_v f_{yt}}{b_w} = \text{Min} \left( \frac{16}{\sqrt{28}}, 3 \right) \frac{226.1 \times 420}{500} = 569.7 \text{ mm}$$

$$s^3_{max} = \frac{A_v f_{yt} d}{\frac{V_u}{\phi} - V_c} = \frac{157.08 \times 420 \times 758}{\frac{530}{0.75} - 299852} = 158.7 \text{ mm}$$

$$s = \text{Min}(s^1_{max}, s^2_{max}, s^3_{max}) = 158.7 \text{ mm}$$

Use  $s = 150$  mm at critical section.

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