

IE-352

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Section 4, CRN: 58626/7/8

Second Semester 1438-39 H (Spring-2018) – 4(4,1,2)

“MANUFACTURING PROCESSES – 2”

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Milling Exercise + ANSWERS

Name: <b>AHMED M. EL-SHERBEENY, PHD</b>	Student Number: 4
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### Material-Removal Rate, Power, Torque, and Cutting Time in Slab Milling

A slab-milling operation is being carried out on a 300 – *mm*-long, 100-*mm*-wide annealed mild-steel block at a feed  $f$  of 0.25 *mm*/tooth and a depth of cut 3.0 *mm*. The cutter is  $D = 50$  *mm* in diameter, has 20 straight teeth, rotates at 100 *rpm* and, by definition, is wider than the block to be machined. Calculate the following:

- material-removal rate,  $MRR$
- estimated power dissipated,  $Power$
- estimated torque required for this operation,  $Torque$
- cutting time,  $t$

Given:

- Process: slab-milling
- Workpiece material: annealed mild-steel
- $l = 300$  *mm*
- $w = 100$  *mm*
- $f = 0.25$  *mm*/tooth
- $d = 3.0$  *mm*
- $D = 50$  *mm*
- $n = 20$
- $N = 100$  *rev*/*min*

Solution:

a) material-removal rate,  $MRR = wdv$

$$f = \frac{v}{Nn}$$

$$\Rightarrow v = fNn = \left(0.25 \frac{\text{mm}}{\text{tooth}}\right) \left(100 \frac{\text{rev}}{\text{min}}\right) \left(20 \frac{\text{teeth}}{\text{rev}}\right) = 500 \text{ mm/min}$$

$$\Rightarrow MRR = wdv = (100 \text{ mm})(3.0 \text{ mm}) \left(500 \frac{\text{mm}}{\text{min}}\right) \left(\frac{1 \text{ min}}{60 \text{ s}}\right) = 2500 \text{ mm}^3/\text{s}$$

►  $MRR = 2500 \text{ mm}^3/\text{s}$

b) power dissipated,  $Power$

remember,  $u_t = \frac{Power}{MRR}$

$u_t$  can be obtained from specific power table in ch. 21, for different workpiece materials

⇒ for mild-steel, we can assume a value of  $3 \text{ W} \cdot \text{s}/\text{mm}^3$

$$\Rightarrow Power = u_t \cdot MRR = \left(3 \frac{\text{W} \cdot \text{s}}{\text{mm}^3}\right) \cdot \left(2500 \frac{\text{mm}^3}{\text{s}}\right) = 7,500 \text{ W}$$

Approximate Range of Energy Requirements in Cutting Operations at the Drive Motor of the Machine Tool (for Dull Tools, Multiply by 1.25)

Material	Specific energy W · s/mm <sup>3</sup>
Aluminum alloys	0.4–1
Cast irons	1.1–5.4
Copper alloys	1.4–3.2
High-temperature alloys	3.2–8
Magnesium alloys	0.3–0.6
Nickel alloys	4.8–6.7
Refractory alloys	3–9
Stainless steels	2–5
Steels	2–9
Titanium alloys	2–5

►  $Power = 7.5 \text{ kW}$

c) torque required,  $Torque$

$$Power = Torque \cdot \omega$$

$$\Rightarrow Torque = \frac{Power}{\omega} = \frac{7500 \text{ W}}{2\pi N} = \frac{7500 \text{ N} \cdot \text{m}/\text{s}}{(2\pi)(100) \text{ rad}/\text{min}} * \frac{60 \text{ s}}{\text{min}} = 716.2 \text{ N} \cdot \text{m}$$

►  $Torque = 716 \text{ N} \cdot \text{m}$

d) **cutting time,  $t$**

$$t = \frac{l + l_c}{v}$$

For  $D \gg d \Rightarrow l_c$  can be approximated using:  $l_c = \sqrt{Dd}$

$$\Rightarrow l_c = \sqrt{Dd} = \sqrt{(50 \text{ mm}) \cdot (3 \text{ mm})} = 12.247 \text{ mm}$$

$$\Rightarrow t = \frac{l + l_c}{v} = \frac{300 \text{ mm} + 12.247 \text{ mm}}{500 \text{ mm/min}} = 0.6245 \text{ min}$$

►  $t = 37.5 \text{ s}$

Note that if we did not do the above assumption for  $l_c$

$$\Rightarrow l_c = \sqrt{d(D - d)} = \sqrt{(3.0 \text{ mm}) \cdot (50 \text{ mm} - 3.0 \text{ mm})} = 11.873 \text{ mm}$$

$$\Rightarrow t = \frac{l + l_c}{v} = \frac{300 \text{ mm} + 11.873 \text{ mm}}{500 \text{ mm/min}} = 0.6237 \text{ min}$$

►  $t = 37.4 \text{ s}$

Thus the above assumption was justified.