

Question 1:

The axial load on building column resulting from the code specified service loads have been calculated as:

$$\begin{aligned}
 P_D &= 530 \text{ kN} \\
 P_L &= 360 \text{ kN} \\
 P_{Lr} &= 178 \text{ kN} \\
 P_W &= 270 \text{ kN (compression)} \\
 &= 310 \text{ kN (tension)}
 \end{aligned}$$

Determine the required strength for this column

Combination	P_u (kN)
Comb.1 → 1.4 D → 1.4 (530)	742
Comb.2 → 1.2 D + 1.6 L + 0.5 L _r → 1.2 (530) + 1.6 (360) + 0.5 (178)	1301
Comb.3(a) → 1.2 D + 1.6 L _r + f ₁ L → 1.2 (530) + 1.6 (178) + 0.5 (360)	1100.8
Comb.3(b) → 1.2 D + 1.6 L _r + 0.8 W → 1.2 (530) + 1.6 (178) + 0.8 (270)	1136.8
Comb.4 → 1.2 D + 1.6 W + f ₁ L + 0.5 L _r → 1.2 (530) + 1.6 (270) + 0.5 (360) + 0.5 (178)	1337
Comb.5 → 1.2 D + 1.0 E + f ₁ L → 1.2 (530) + 1.0 (0) + 0.5 (360)	816
Comb.6(a) → 0.9 D + 1.6 W → 0.9 (530) + 1.6 (270)	909
Comb.6(b) → 0.9 D - 1.6 W → 0.9 (530) - 1.6 (310)	-19
Comb.7 → 0.9 D + 1.0 E → 0.9 (530) + 1.0 (0)	477

Based on combination results, the required strength of the column is **1337 kN in compression** and **19 kN in tension**.

Question 2:

Compute the net area for each of given member .assume 22-mm bolts.

(a)

$$d_b = 22 \text{ mm}$$

$$t = 16 \text{ mm}$$

$$A_g = 300 \times 16 = 4800 \text{ mm}^2$$

Path 1-1:

$$A_n = A_g - \sum (d_b + 3 \text{ mm}) t$$

$$A_n = 4800 - 3 (25)(16) = \mathbf{3600 \text{ mm}^2}$$

Path 2-2:

$$A_n = A_g - \sum (d_b + 3 \text{ mm}) t + \sum \frac{s^2}{4g} t$$

$$A_n = 4800 - 4 (25)(16) + 2 \frac{(75)^2}{4(50)} (16)$$

$$A_n = 4800 - 1600 + 900 = \mathbf{4100 \text{ mm}^2}$$

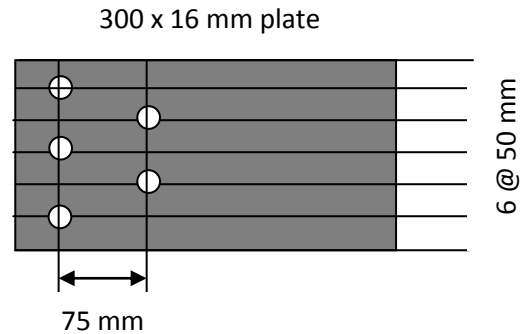
Path 3-3:

$$A_n = A_g - \sum (d_b + 3 \text{ mm}) t + \sum \frac{s^2}{4g} t$$

$$A_n = 4800 - 5 (25)(16) + 4 \frac{(75)^2}{4(50)} (16)$$

$$A_n = 4800 - 2000 + 1800 = \mathbf{4600 \text{ mm}^2}$$

\therefore **Critical $A_n = 3600 \text{ mm}^2$**



(b)

$$d_b = 22 \text{ mm}$$

$$t = 16 \text{ mm}$$

$$A_g = 400 \times 16 = 6400 \text{ mm}^2$$

Path 1-1:

$$A_n = A_g - \sum (d_b + 3 \text{ mm}) t$$

$$A_n = 6400 - 3 (25)(16) = \mathbf{5200 \text{ mm}^2}$$

Path 2-2:

$$A_n = A_g - \sum (d_b + 3 \text{ mm}) t + \sum \frac{s^2}{4g} t$$

$$A_n = 6400 - 4 (25)(16) + 2 \frac{(75)^2}{4(60)} (16)$$

$$A_n = 6400 - 1600 + 750 = \mathbf{5550 \text{ mm}^2}$$

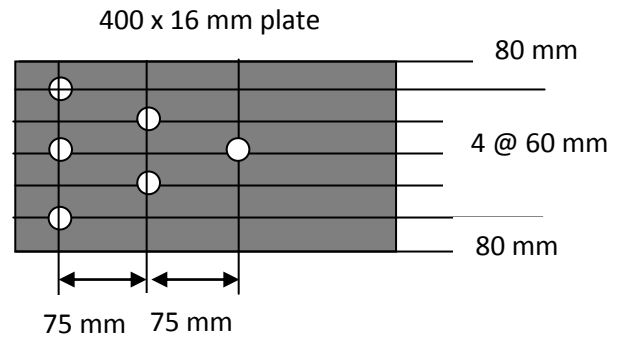
Path 3-3:

$$A_n = A_g - \sum (d_b + 3 \text{ mm}) t + \sum \frac{s^2}{4g} t$$

$$A_n = 6400 - 5 (25)(16) + 4 \frac{(75)^2}{4(60)} (16)$$

$$A_n = 6400 - 2000 + 1500 = \mathbf{5900 \text{ mm}^2}$$

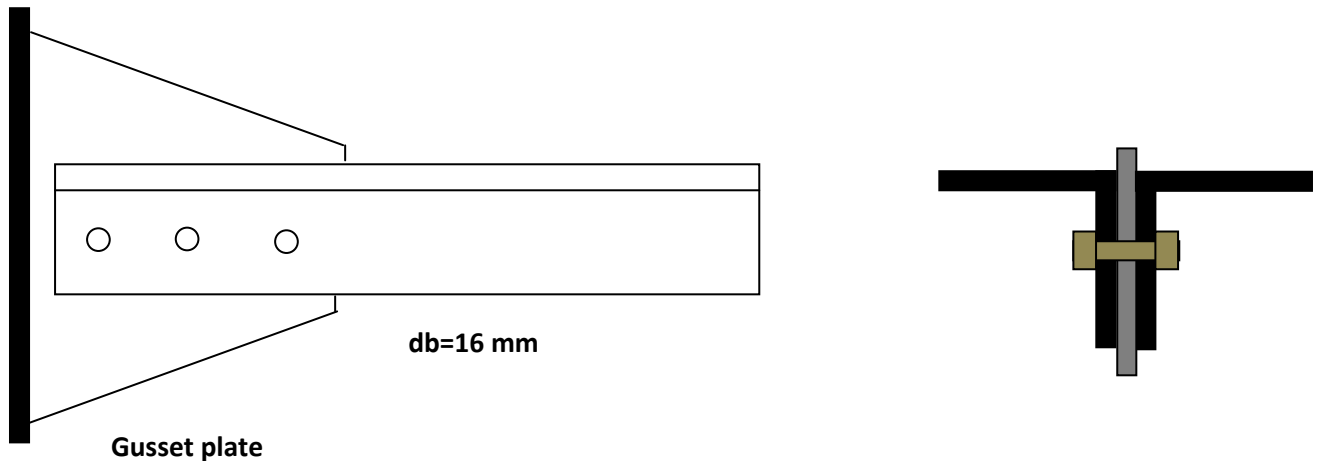
$$\therefore \text{Critical } A_n = \mathbf{5200 \text{ mm}^2}$$



Question 3:

Two A36 L102x102x9.5 are connected to gusset plate with 16mm diameter bolts, as shown in figure below. Compute the tensile strength of the member.

Assume that the $A_e=85\%$ of A_n .



Gross area of angle = $A_g = 3700 \text{ mm}^2$ (Table on page 1-86 of AISC Manual)

$t = 9.5 \text{ mm}$

A36M steel: $F_y=250 \text{ MPa}$

$F_u=400 \text{ MPa}$

Net section area:

$d_b=16\text{mm}$

$$A_n = 3700 - 2(16 + 3) \times 9.5 = 3339 \text{ mm}^2$$

Effective net area:

$$A_e = 0.85 \times 3339 = 2838.15 \text{ mm}^2$$

Gross yielding design strength = $\phi_t A_g F_y = 0.9 \times 3700 \times 250 \times 10^{-3} = \mathbf{832.5 \text{ kN}}$

Net section fracture = $\phi_t A_e F_u = 0.75 \times 2838.15 \times 400 \times 10^{-3} = 851.445 \text{ kN}$

Design strength $\phi_t P_n = 832.5 \text{ kN}$ (gross yielding governs)