

//

:	:
---	---

() : (x) (✓)

(d_g)

(T_r)

(ET_d)

(E_{cemin})

(SDR)

pH

%

q_{var}

() :

%

%

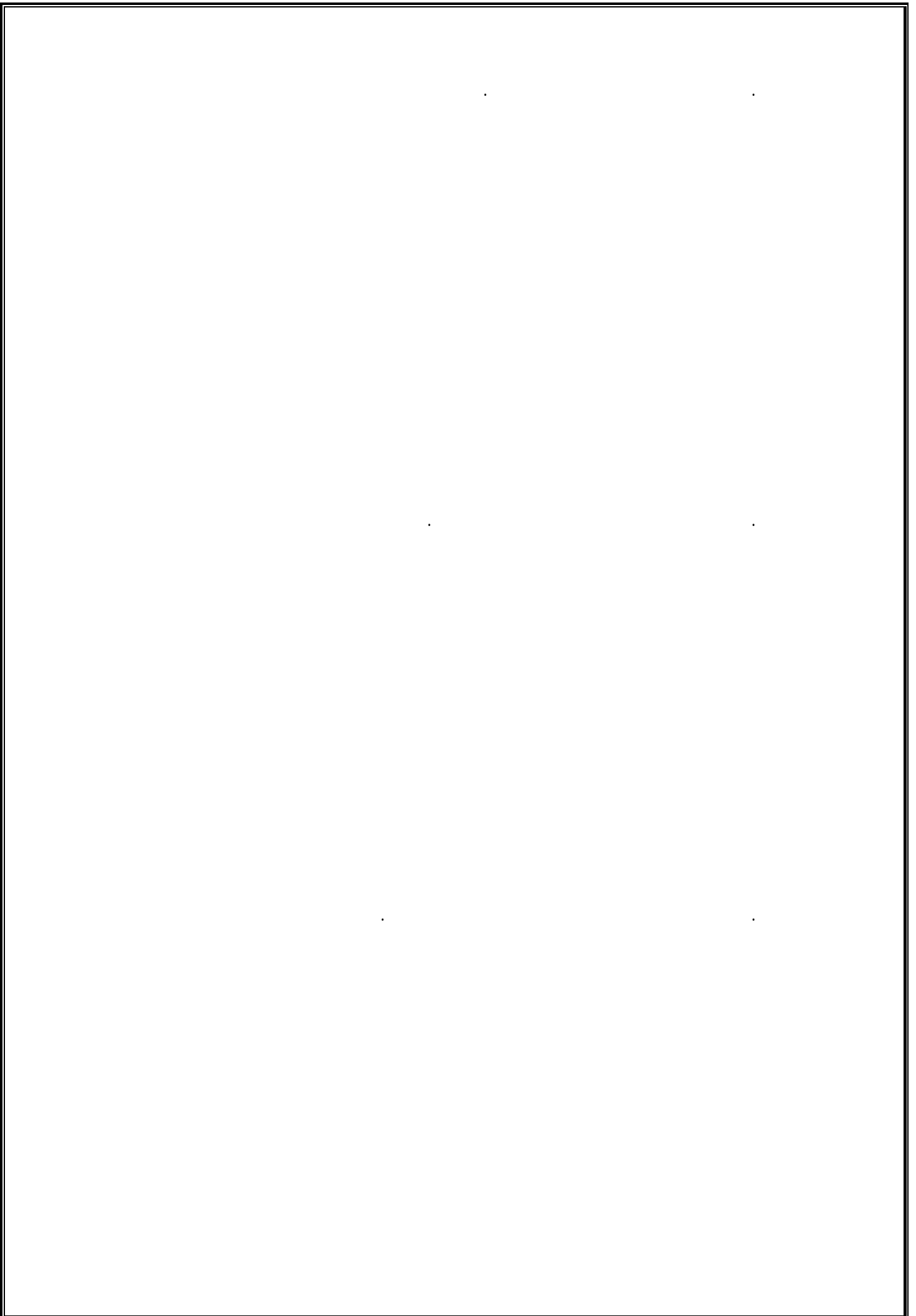
%

%

d_p

$$V_p = d_p^2 \cdot g \cdot (\rho_p - \rho_w) / 18 \cdot \mu$$

():



() :

(B)

المنظارات الدوامة:
$$f = 3.6 \times 0.4 \times \frac{\pi}{4} (0.6)^2 \times (15)^{0.4} \sqrt{2 \times 9.81} = 5.327 \text{ L/hr}$$

المنظارات ذات النوصة:

$$5.327 = 3.6 \times 0.8 \times \frac{\pi}{4} d^2 \sqrt{2 \times 9.81 \times 15}$$

$$\therefore d = 0.37 \text{ mm}$$

المنظارات سائلة الضغط:
$$5.327 = 3.6 \times 0.6 \times \frac{\pi}{4} d^2 (15)^{0.2} \sqrt{2 \times 9.81}$$

$$\therefore d = 0.642 \text{ mm}$$

المنظارات ذاتية السيل المتر:

$$5.327 = 3.6 \times 0.65 \times \frac{\pi}{4} d^2 \times \left(\frac{15}{4}\right)^{0.7} \sqrt{2 \times 9.81}$$

$$d = 0.51 \text{ mm}$$

المنظارات ذات السار الطويل:

$$5.327 = \frac{0.866 \times 15 \times d^4}{0.24}$$

$$\therefore d = 0.56 \text{ mm}$$

() %

$$V_p = q_c \times N_p \times t_a$$

$$280 = 4 \times N_p \times 16$$

$$\therefore N_p = 4.37 = \underline{5}$$

$$t_{aa} = \frac{280}{4 \times 5} = \underline{14 \text{ hr}}$$

$$Q_L = N_{tree} \times N_p \times q_c$$

$$= 40 \times 5 \times 4 = 800 \text{ L/hr} = 0.222 \text{ L/s}$$

$$L = N_{tree} \times S_p = 40 \times 6 = 240 \text{ m}$$

$$\Delta H_L = 0.55 \Delta H_S = 0.55 \times 6 = 3.3 \text{ m}$$

$$\therefore 3.3 = H_f - \frac{1}{100} \times 240$$

$$\therefore H_f = 5.7 \text{ m}$$

$$\therefore 5.7 = 3.98 \times 10^5 \times 240 \frac{(0.222)^{1.852}}{D^{4.871}}$$

$$\therefore D = \underline{17 \text{ mm}}$$

$$Q_3 = \frac{100}{5} \times 4 \times \frac{8}{360} = 0.177 \text{ L/s}$$

$$Q_2 = 2Q_3 = 0.363 \text{ L/s}$$

$$Q_1 = 3Q_3 = 0.533 \text{ L/s}$$

$$\left(\frac{\sum \ell/L \right) \quad () \quad (\Delta H/H_i) \quad :$$

$$(L/H_i) \quad (\sum \Delta H_e/L)$$

$$\frac{L}{H_i} = \frac{300}{12} = 25$$

Sect:	ℓ_m	$\sum \ell$	$\frac{\sum \ell}{L}$	S	ΔH_e	$\sum \Delta H_e$	$\frac{\sum \Delta H_e}{L}$	$\frac{\Delta H}{H_i}$	Loss % at $\frac{\Delta H}{H_i} = 0.45$
1	100	100	0.33	4.5↑	+4.5	4.5	0.015	0.40	- 8%
2	100	200	0.66	1.5↓	-1.5	3.0	0.010	0.45	0
3	100	300	1.0	3.0↑	+3.0	6.0	0.020	0.55	17%

$$(\Delta H/H_i)$$

()

$$(\Delta H/L) \quad (\Delta H) \quad (\% \pm)$$

$$\Delta H = 0.45 H_i = 0.45 \times 12 = 5.4$$

$$\Delta H/L = 5.4/300 = 0.018 = 1.8\%$$

(Q)

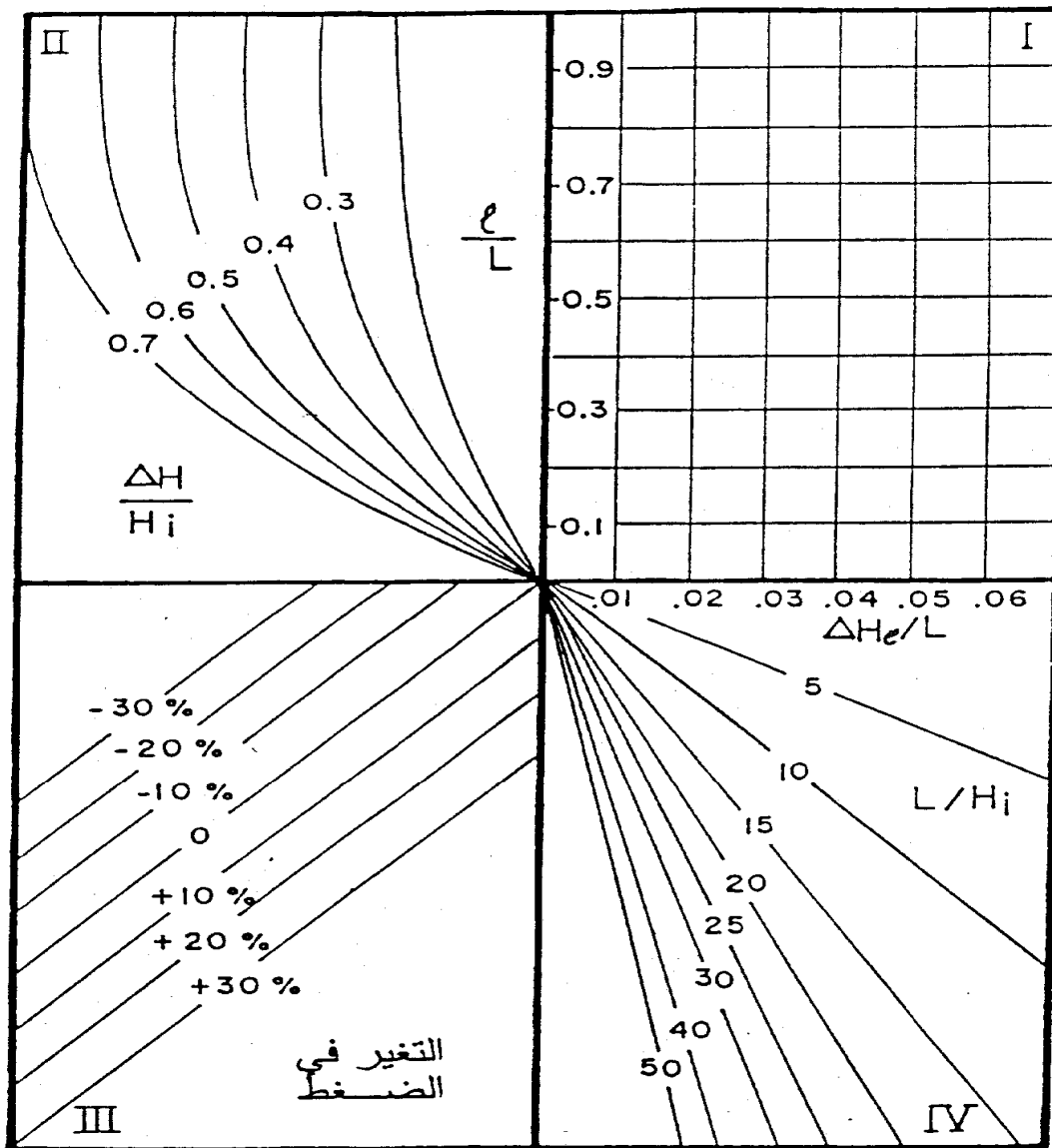
()

$$(\Delta H/L)$$

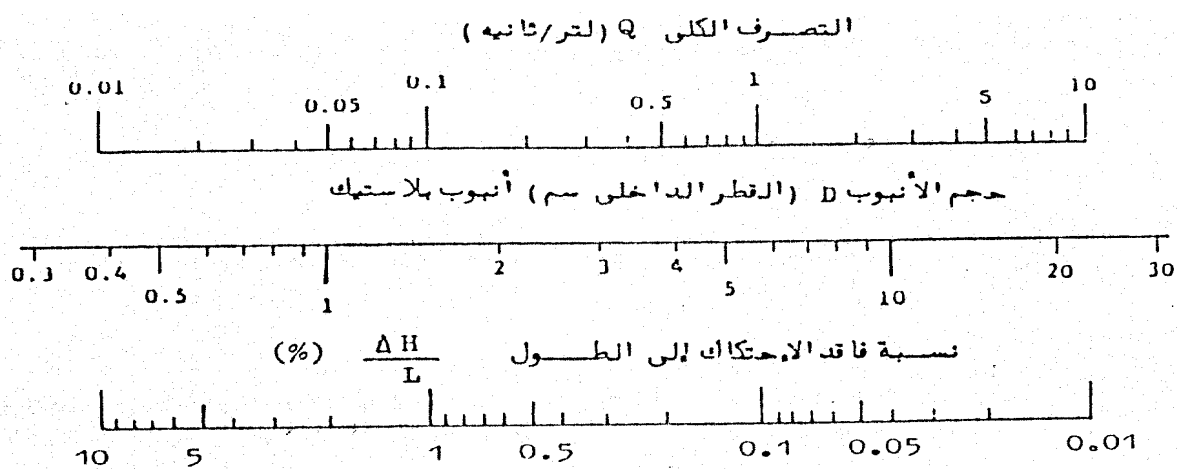
$$D_1 = 26 \text{ mm}$$

$$D_2 = 21 \text{ mm}$$

$$D_3 = 17 \text{ mm}$$



()



()

%

β

$$r_{var} = \frac{r_m - r_n}{r_m} = 1 - \frac{r_n}{r_m} \quad \therefore 0.20 = 1 - \frac{r_n}{r_m} \quad \therefore \frac{r_n}{r_m} = 0.80$$

$$\therefore r_{ca} = 0.87 r_m$$

$$\therefore \frac{r_n}{r_a / 0.87} = 0.80 \quad \therefore \frac{r_n}{r_a} = \frac{0.80}{0.87} = 0.92$$

$$\therefore E U_f = \underline{92\%} \quad \textcircled{1}$$

$$U_s = (1 - 0.12) \times 100 = (1 - 0.12) \times 100 = \underline{88\%} \quad \textcircled{4}$$

$$E U_d = \left(1 - \frac{1.27 \times 0.12}{\sqrt{3}}\right) \times 0.92 \times 100 = \underline{83.9\%} \quad \textcircled{3}$$

$$E U_a = \frac{1}{2} \left(\frac{r_n}{r_a} + \frac{r_n}{r_m}\right) \times 100 = \frac{1}{2} (0.92 + 0.87) \times 100 = \underline{89.5\%} \quad \textcircled{3}$$

$$C_{h_h} = \frac{c_v}{\beta} = \frac{0.12}{0.6} = 0.20 \quad U_{sh} = (1 - C_{h_h}) \times 100 = (1 - 0.20) \times 100 = \underline{80\%} \quad \textcircled{5}$$

$$C_{h_p} = \sqrt{c_v^2 + c_p^2} = \sqrt{0.12^2 + 0.09} = 0.15 \quad \therefore U_{sp} = (1 - C_{h_p}) \times 100 = (1 - 0.15) \times 100$$

$$\therefore U_{sp} = \underline{85\%} \quad \textcircled{6}$$

$$C_{h_t} = \sqrt{0.15^2 + 0.20^2} = 0.25 \quad U_{st} = \underline{75\%} \quad \textcircled{7}$$

$$0.20 = L (1 - H_{var})^{0.6} \quad H_{var} = \underline{0.31} \quad \textcircled{8}$$