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$$H_{ss} = -2 \text{ m}$$

$$d = 75 \text{ mm}$$

$$H_{sd} = 3 \text{ m}$$

$$h_p = 0$$

$$Q = 25 \text{ L/s}$$

$$h_{\text{total}} = 5 \text{ m}$$

$$E = 70\%$$

$$N = 1500 \text{ RPM}$$

$$BP = ?$$

$$N_s = ?$$

الضغط عند الارتفاعات المتساوية

$$H_{st} = H_{sd} - H_{ss} = 3 - 2 = 1 \text{ m}$$

$$h_p = 0$$

$$V = \frac{Q}{A} = \frac{0.025}{\frac{\pi}{4}(0.075)^2} = 5.66 \text{ m/s}$$

$$h_v = \frac{V^2}{2g} = \frac{(5.66)^2}{2 \times 9.81} = 1.63 \text{ m}$$

الضغط عند الارتفاعات المتساوية

$$\begin{aligned} TDH = H &= H_{st} + h_f + h_v + h_p \rightarrow 0 \\ &= 1 + 5 + 1.63 \\ &= 7.63 \text{ m} \end{aligned}$$

القدرة اللازمة لتشغيل المضخة

$$BP = \frac{Q \times H}{102 \times E} = \frac{25 \times 7.63}{102 \times 0.70} = \underline{2.67 \text{ kW}}$$

السرعة النوعية للمضخة

$$N_s = 0.2108 N \frac{Q^{0.5}}{H^{0.75}}$$

$$= 0.2108 \times 1500 \frac{(25 \times 60)^{0.5}}{(7.63)^{0.75}}$$

$$= \underline{2668 \text{ Unit}}$$

$N_1 = 1500 \text{ rpm}$  ,  $D_1 = 0.32 \text{ m}$  ,  $Q_1 = 20 \text{ lit/sec}$  ,  $H_1 = 16.8 \text{ m}$  ,  $PB_1 = 4.5 \text{ kw}$

$N_2 = 1750 \text{ rpm}$  ,  $D_2 = 0.38 \text{ m}$  ,  $Q_2 = ??$  ,  $H_2 = ??$  ,  $PB_2 = ??$

$$H_2 = H_1 \left( \frac{N_2 \cdot D_2}{N_1 \cdot D_1} \right)^2 = 16.8 * \left( \frac{1750 * 0.38}{1500 * 0.32} \right)^2 = 32.25 \text{ m}$$

$$Q_2 = Q_1 \left( \frac{N_2}{N_1} \right) \left( \frac{D_2}{D_1} \right)^3 = 20 * \left( \frac{1750}{1500} \right) \left( \frac{0.38}{0.32} \right)^3 = 39.1 \frac{\text{lit}}{\text{sec}}$$

$$PB_2 = PB_1 \left( \frac{N_2}{N_1} \right)^3 \left( \frac{D_2}{D_1} \right)^5 = 4.5 * \left( \frac{1750}{1500} \right)^3 \left( \frac{0.38}{0.32} \right)^5 = 16.87 \text{ kw}$$

$$WP_2 = \frac{Q_2 \times H_2}{102} = \frac{39.1 \times 32.25}{102} = 12.36 \text{ kw}$$

$$E_2 = \frac{WP_2}{PB_2} \times 100 = \frac{12.36}{16.87} \times 100 = 73.3\%$$

$$N_{s2} = 0.2108 N_2 \left( \frac{Q_2^{0.5}}{H_2^{0.75}} \right) = 0.2108 \times 17500 \times \frac{(39.1 \times 60)^{0.5}}{32.25^{0.75}} = 1320 \text{ unit}$$

$$H_{SS} = 6 \text{ m} \quad h_{LS1} = 0.375 \text{ m} \quad h_{FS} = 0.75 \text{ m} \quad h_V = 0.25 \text{ m}$$

$$h_P = 0 \quad P_{atmos} = 1.03 \text{ Kg/cm}^2 \quad P_V = 0.05 \text{ Kg/cm}^2$$

أي المقومات تحتها

$$a) N_S = 1000 \text{ unit} \quad \sigma = 0.25$$

$$b) N_S = 2500 \text{ unit} \quad \sigma = 0.35$$

الرباعية الدنيا من الكلف

$$H = H_{st} + h_f + h_p + h_v$$

$$= (H_{s1} + H_{s2}) + (h_{f1} + h_{f2}) + h_p + h_v$$

دعيت المصفاة تفرغ مباشرة نحو الهواء فيكون  $h_{s1} = 0$  و  $h_{f1} = 0$  و  $h_p = 0$

$$\therefore H = (0 + 6) + (0.375 + 0.75) + 0 + 0.25$$

$$= 7.375 \text{ m}$$

سبب الصفاف الموجب المطلوب لكل مصفاة حتى لا يحد من كلفها بها

$$NPSHR_a = \sigma_1 \times H = 0.25 \times 7.375 = 1.844 \text{ m}$$

$$NPSHR_b = \sigma_2 \times H = 0.35 \times 7.375 = 2.581 \text{ m}$$

صافط السبب الصفاف الموجب الموتر للنظام

$$NPSHA = P_{atmos} - H_{SS} - h_{FS} - P_V$$

$$= (1.03 \times 10) - 6 - (0.375 + 0.75 + 0.25) - (0.05 \times 10)$$

$$= 10.3 - 6 - 1.375 - 0.50$$

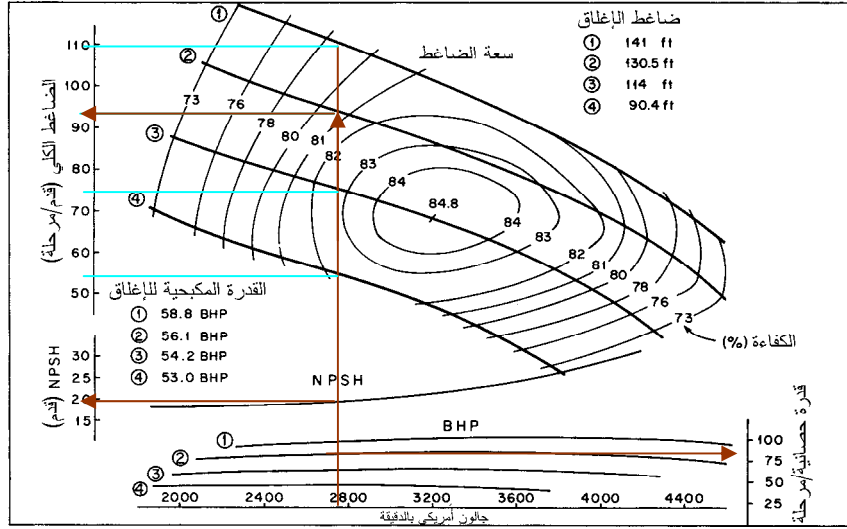
$$= \underline{2.425 \text{ m}}$$

$$\therefore NPSHR_b > NPSHA$$

∴ حدت تكلفت عند استخدام المصفاة b فهي لا تصلح لهذا النظام

$$\therefore NPSHR_a < NPSHA$$

∴ لديت تكلفت عند استخدام المصفاة a فهي تصلح لهذا النظام



$$H/\text{stage} = 110 \text{ ft}$$

$$H_t = 110 \text{ ft}/\text{stage} (1 \text{ stage}) = 110 \text{ ft}$$

$$H_t < H_d$$

$$H/\text{stage} = 93 \text{ ft}$$

$$H_t = 93 \text{ ft}/\text{stage} (2 \text{ stages}) = 186 \text{ ft}$$

$$H_t > H_d$$

$$H/\text{stage} = 93 \text{ ft} = 28.35 \text{ m}$$

$$Q = 2800 \text{ gal}/\text{min} = 176.63 \text{ Lit}/\text{sec}$$

$$P/\text{stage} = 81 \text{ hp} (0.7457 \text{ kw}/\text{hp}) = 60.4 \text{ kw}$$

$$P_T = 60.4 \text{ kw}/\text{stage} (2 \text{ stages}) = 120.8 \text{ kw}$$

$$\text{NPSHR} = 19 \text{ ft} = 5.79 \text{ m}$$

$$E = 0.81 = 81 \%$$

$$BP = \frac{QH}{102E} = \frac{176.63 \times 28.35}{102 \times 0.81} = 60.61 \text{ kw}$$